Optimization-based Control of Hybrid Dynamical Systems

Alberto Bemporad

http://www.dii.unisi.it/~bemporad



Department of Information Engineering



COHES Group



Control and Optimization of Hybrid and Embedded Systems

Contents

- Models of hybrid systems
- Model predictive control of hybrid systems
- Explicit reformulation
- Automotive applications

Hybrid Systems



Hybrid Systems



IEEE TRANSACTIONS ON AUTOMATIC CONTROL

VOL. AC-11, NO. 2

APRIL, 1966

A Class of Hybrid-State Continuous-Time Dynamic Systems

H. S. WITSENHAUSEN

Abstract—A class of continuous time systems with part continuous, part discrete state is described by differential equations combined with multistable elements. Transitions of these elements between their discrete states are triggered by the continuous part of the state and not directly by inputs. The dynamic behavior of such systems, in response to piecewise continuous inputs, is defined under suitable assumptions. A general Mayer-type optimization problem is formulated. Conditions are given for a solution to be well-behaved, so that variational methods can be applied. Necessary conditions for optimality are stated and the jump conditions are interpreted geometrically.

INTRODUCTION

gates to process Boolean signals, 3) electronic analog switches controlled by Boolean signals.

The objective of this paper is to give a precise description of such systems, to define their dynamics, to formulate the problem of their optimum control, to introduce the notion of well-behaved solution, and to state necessary conditions for optimality (the jump conditions).

A CLASS OF HYBRID SYSTEMS

OME PHYSICAL objects evolve in time according

The modifications required in otherwise continuous systems described by vector differential equations

Embedded Systems



- Consumer electronics
- Home appliances
- Oce automation
- Automobiles
- Industrial plants

Motivation: "Intrinsically Hybrid"



• Transmission

Discrete command (R,N,1,2,3,4,5) Continuous dynamical variables (velocities, torques)



• Four-stroke engines

+

Automaton, dependent on power train motion



Key Requirements for Hybrid Models

• Descriptive enough to capture the behavior of the system

- continuous dynamics (physical laws)
- logic components (switches, automata, software code)
- interconnection between logic and dynamics

• Simple enough for solving analysis and synthesis problems

linear hybrid systems

"Make everything as simple as possible, but not simpler." — Albert Einstein



Piecewise Ane Systems



 $x \in \mathcal{X} \subseteq \mathbb{R}^n$, $u \in \mathcal{U} \subseteq \mathbb{R}^m$, $y \in \mathcal{Y} \subseteq \mathbb{R}^p$ $i(k) \in \{1, \dots, s\}$

(Sontag 1981)

Can approximate nonlinear and/or discontinuous dynamics arbitrarily well



Discrete Hybrid Automaton

(Torrisi, Bemporad, 2004)



 $x_{\ell} \in \{0, 1\}^{n_b} = \text{binary states}$ $u_{\ell} \in \{0, 1\}^{m_b} = \text{binary inputs}$ $\delta_e \in \{0, 1\}^{n_e} = \text{event variables}$ $x_c \in \mathbb{R}^{n_c} = \text{continuous states}$ $u_c \in \mathbb{R}^{m_c} = \text{continuous inputs}$ $i \in \{1, 2, \dots, s\} = \text{current mode}$

Switched Ane System



The ane dynamics depend on the current mode i(k):

$$x_c(k+1) = A_{i(k)}x_c(k) + B_{i(k)}u_c(k) + f_{i(k)}$$

 $x_c \in \mathbb{R}^{n_c}, \ u_c \in \mathbb{R}^{m_c}$

Event Generator



Event variables are generated by linear threshold conditions over continuous states, continuous inputs, and time:

$$[\delta_e^i(k) = 1] \leftrightarrow [H^i x_c(k) + K^i u_c(k) \le W^i]$$

 $x_c \in \mathbb{R}^{n_c}, \ u_c \in \mathbb{R}^{m_c}, \ \delta_e \in \{0, 1\}^{n_e}$

Example: $[\delta(k)=1] \leftrightarrow [x_c(k)\geq 0]$

Finite State Machine



The binary state of the nite state machine evolves according to a Boolean state update function:

$$x_{\ell}(k+1) = f_{\mathsf{B}}(x_{\ell}(k), u_{\ell}(k), \delta_{e}(k))$$

$$x_\ell \in \{0,1\}^{n_\ell}, \ u_\ell \in \{0,1\}^{m_\ell}, \ \delta_e \in \{0,1\}^{n_e}$$

Example: $x_{\ell}(k+1) = \neg \delta_e(k) \lor (x_{\ell}(k) \land u_{\ell}(k))$

Mode Selector



The mode selector can be seen as the output function of the discrete dynamics

The active mode i(k) is selected by a Boolean function of the current binary states, binary inputs, and event variables:

$$i(k) = f_{\mathsf{M}}(x_{\ell}(k), u_{\ell}(k), \delta_{e}(k))$$

$$x_\ell \in \{0,1\}^{n_\ell}, \ u_\ell \in \{0,1\}^{m_\ell}, \ \delta_e\{0,1\}^{n_e}$$

Example: $i(k) = \begin{bmatrix} \neg u_{\ell}(k) \lor x_{\ell}(k) \\ u_{\ell}(k) \land x_{\ell}(k) \end{bmatrix} \longrightarrow \frac{\frac{u_{\ell}/x_{\ell}}{0} \quad 0 \quad 1}{1 \quad i = \begin{bmatrix} 1 \\ 0 \end{bmatrix}}$

the system has 3 modes



Mixed Logical Dynamical Systems

Discrete Hybrid Automaton



- Computationally oriented (mixed-integer programming)
- Suitable for controller synthesis, verication, ...

Hybrid Toolbox for Matlab

<u>Features:</u>

(Bemporad, 2003-2006)

- Hybrid model (MLD and PWA) design, simulation, verication
- Control design for linear systems w/ constraints and hybrid systems (on-line optimization via QP/MILP/MIQP)
- Explicit control (via multiparametric programming)



http://www.dii.unisi.it/hybrid/toolbox

Mixed-Integer Models in OR

Translation of logical relations into linear inequalities is heavily used in operations research (OR) for solving complex decision problems by using mixed-integer (linear) programming (MIP)

<u>Example</u>: Optimal multi-period investments for maintenance and upgrade of electrical energy distribution networks



(Bemporad, Muñoz, Piazzesi, 2006)

Example: Timetable generation (for demanding professors ...)

	8	9	10	11	12	13	14	15	16	17	18	19
lun		Sistemi Operativi (*18)					Moure per la Automazione ("7)		Ingegneria del Software (*18)			
							Bas	i di Dati (*18)				
mar		Bas	i di Dati (*3)	Sistemi	Operativi (*3)		Robotica	ed Automazione di loesso (*18)				T
mer		Robotica Po	ed Automazione di ocesso (*8)	Ms	ure per la nazione (*7)		Laboratorio di Vile		Robotic cale (*15	a e Realtà)		
			Ingegneria del So	ftware (*	10)							
gio	Π	Basi di Dati (*3)					Sisten	i Operativi (*5)				
		Laboratorio di Robotica e Realtà Vituale (*15)										
ven	Π	Robotica ed Automazione di Processo (*8)					Moure per la Automazione (??)					
		ing Se	pegnerta del fovare (*18)									T
sab												



CPU time: 0.2 s

Major Advantages of Linear Hybrid Models

Many problems of analysis:

- Stability
- Safety / Reachability
- Observability
- Passivity

(Johansson, Rantzer, 1998)

(Torrisi, Bemporad, 2001)

(Bemporad, Ferrari-Trecate, Morari, 2000)

(Bemporad, Bianchini, Brogi, 2006)

Many problems of synthesis:

- Controller design (Bemporad, Morari, 1999)
- Robust control design (Silva, Bemporad, Botto, Sá da Costa, 2003)
- Filter design (state estimation/fault detection)

(Bemporad, Mignone, Morari, 1999)

(Ferrari-Trecate, Mignone, Morari, 2002)

(Pina, Botto, 2006)

can be solved through mathematical programming

(However, all these problems are NP-hard !)

Contents

- ✓ Models of hybrid systems
- Model predictive control of hybrid systems
- Explicit reformulation
- Automotive applications

Hybrid Control Problem

hybrid process



MPC for Hybrid Systems



Model Predictive (MPC) Control

• At time t solve with respect to $U \triangleq \{u(t), u(t+1), \dots, u(t+T-1)\}$ the nite-horizon open-loop, optimal control problem:

$$\min_{\substack{u(t),...,u(t+T-1) \\ +\sigma(\|\delta(t+k) - \delta_r\| + \|z(t+k) - z_r\| + \|x(t+k|t) - x_r\|)} } \sum_{k=0}^{T-1} \|y(t+k|t) - r(t)\| + \rho \|u(t+k) - u_r\| \\ +\sigma(\|\delta(t+k) - \delta_r\| + \|z(t+k) - z_r\| + \|x(t+k|t) - x_r\|)$$
subject to MLD model
$$x(t|t) = x(t) \\ x(t+T|t) = x_r$$

• Apply only $u(t) = u^*(t)$ (discard the remaining optimal inputs)

• Repeat the whole optimization at time t+1

Closed-Loop Convergence

Theorem 1 Let $(x_r, u_r, \delta_r, z_r)$ be the equilibrium values corresponding to the set point r, and assume x(0) is such that the MPC problem is feasible at time t = 0. Then $\forall Q, R \succ 0, \forall \sigma > 0$

$$\lim_{t\to\infty} y(t) = r$$
$$\lim_{t\to\infty} u(t) = u_r$$
$$\lim_{t\to\infty} x(t) = x_r, \ \lim_{t\to\infty} \delta(t) = \delta_r, \ \lim_{t\to\infty} z(t) = z_r,$$
and all constraints are fulfilled.

(Bemporad, Morari 1999)

Proof: Easily follows from standard Lyapunov arguments

More stability results: see (Lazar, Heemels, Weiland, Bemporad, 2006)

Hybrid MPC - Example

<u>PWA system:</u>

$$\begin{aligned} x(t+1) &= 0.8 \begin{bmatrix} \cos \alpha(t) & -\sin \alpha(t) \\ \sin \alpha(t) & \cos \alpha(t) \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t) \\ y(t) &= x_2(t) \\ \alpha(t) &= \begin{cases} \frac{\pi}{3} & \text{if } x_1(t) > 0 \\ -\frac{\pi}{3} & \text{if } x_1(t) \le 0 \end{cases} \end{aligned}$$

<u>Constraint:</u> $-1 \le u(t) \le 1$

Open loop behavior



/demos/hybrid/bm99sim.m

Hybrid MPC - Example

Closed loop:



k=1

24

ime offset: 0



Event-based Continuous-time Hybrid Automaton (icHA)



Switched integral dynamics

$$\frac{dx_c(t)}{dt} = B_{i(t)}u_c(t) + f_{i(t)}$$

k = event counter

Asynchronous FSM

 $x_i(k)$

 $u_l(k) = \delta_c(k)$

 $u_c(k)$

Mode Selector

r.(k

mode i(k)

 $\delta_e(k)$

 $u_i(k)$

Optimal Control of Hybrid Systems: Computational Aspects

MPC for Linear Systems

Linear model

Quadratic
performance index
$$\min_{U} J(x(t), U) = \sum_{k=0}^{N-1} \left[x'_k Q x_k + u'_k R u_k \right] + x'_N P x_N$$

 $\begin{array}{ll} \text{Constraints} & \left\{ \begin{array}{l} u_{\min} \leq u_k \leq u_{\max} \\ y_{\min} \leq y_k \leq y_{\max} \end{array} \right. \end{array} \right.$

This is a (convex) Quadratic Program (QP)

MIQP Formulation of MPC

(Bemporad, Morari, 1999)

$$\min_{\xi} J(\xi, x(0)) = \sum_{t=0}^{T-1} y'(t)Qy(t) + u'(t)Ru(t) \\ \text{subject to} \begin{cases} x(t+1) = Ax(t) + B_1u(t) + B_2\delta(t) + B_3z(t) + B_5 \\ y(t) = Cx(t) + D_1u(t) + D_2\delta(t) + D_3z(t) + D_5 \\ E_2\delta(t) + E_3z(t) \leq E_4x(t) + E_1u(t) + E_5 \end{cases}$$

• Optimization vector:

$$\xi = [u(0), \dots, u(T-1), \delta(0), \dots, \delta(T-1), z(0), \dots, z(T-1)]'$$

$$\implies \min \frac{1}{2} \xi' H\xi + x(0)'F\xi + \frac{1}{2} x'(0) Y x(0)$$

Subj. to $G\xi \leq W + Sx(t)$
$$= u \in \mathbb{R}^{n_u}, \ \delta \in \{0,1\}^{n_\delta}, \ z \in \mathbb{R}^{n_z} \implies \xi \in \mathbb{R}^{(n_u+n_z)T} \times \{0,1\}^{n_\delta T}$$

 ξ has both real and $\{0,1\}$ components

MILP Formulation of MPC

(Bemporad, Borrelli, Morari, 2000)

$$\label{eq:min} \min_{\xi} \ J(\xi, x(0)) = \sum_{t=0}^{T-1} \|Qy(t)\|_\infty + \|Ru(t)\|_\infty$$
 subject to MLD model

- Basic trick: introduce $\min_{x} |x| \implies \min_{x,\epsilon} \epsilon$ slack variables: $s.t. \epsilon \ge x$ $\epsilon \ge -x$
- Generalization: $\begin{cases} \epsilon_k^x \ge \|Qy(t+k|t)\|_{\infty} \\ \epsilon_k^u \ge \|Ru(t+k)\|_{\infty} \end{cases}$
- Optimization vector:

 $\xi = [\epsilon_1^x, \dots, \epsilon_{T-1}^x, \epsilon_0^u, \dots, \epsilon_{T-1}^u, u(0), \dots, u(T-1), \delta(0), \dots, \delta(T-1), z(0), \dots, z(T-1)]'$

$$\min_{\xi} J(\xi, x(0)) = \sum_{k=0}^{T-1} \epsilon_i^x + \epsilon_i^x$$

s.t. $G\xi \le W + Sx(0)$

Mixed Integer Linear Program (MILP)

 ξ has both real and $\{0,1\}$ components

Mixed-Integer Program Solvers

• Mixed-Integer Programming is NP-hard

BUT

• Extremely rich literature in Operations Research (still very active)

MILP/MIQP is nowadays a technology (CPLEX, Xpress-MP, BARON, GLPK, see e.g. <u>http://plato.la.asu.edu/bench.html</u> for a comparison)

- No need to reach the global optimum for stability of MPC (see proof of the theorem), although performance deteriorates
- Possibility of combining symbolic + numerical solvers Example: SAT + linear programming

2000-000	42002001	Sat ins	tances	Unsat instances		
N. Vars	N. Cons	ZCHAFF	CPLEX	ZCHAFF	CPLEX	
20	91	0	0.036	-	-	
50	218	0	0.343	0	0.453	
75	325	0	0.203	0	3.671	
100	430	0	23.328	0	33.921	
125	538	0.016	15.171	0.031	209.766	
150	645	0.031	20.625	0.281	4949.58	
175	753	0.031	> 1500	0.891	> 5000	



Contents

- ✓ Models of hybrid systems
- ✓ Model predictive control of hybrid systems
- Explicit reformulation
- Automotive applications
- Hybrid MPC over wireless sensor networks

On-Line vs O-Line Optimization

$$\begin{split} \min_{U} J(U,x(t)) &= \sum_{k=0}^{T-1} \|Rx(t+k|t)\|_p + \|Qu(t+k)\|_p\\ \text{subject to} \begin{cases} \mathsf{MLD model}\\ x(t|t) = x(t) \end{cases} \end{split}$$

• On-line optimization: given x(t) solve the problem at each time step t.

Mixed-Integer Linear/Quadratic Program (MILP/MIQP)

- Good for large sampling times (e.g., 1 h) / expensive hardware but not for fast sampling (e.g. 10 ms) / cheap hardware !
- O-line optimization: solve the MILP/MIQP for all x(t)

$$\min_{\zeta} J(\zeta, x(t)) = \begin{cases} f'\zeta & \infty \text{-norm} \\ \zeta' H \zeta + f'\zeta & 2\text{-norm} \end{cases}$$

s.t. $G\zeta \le W + Fx(t)$

multi-parametric programming

Example of Multiparametric Solution

Multiparametric LP ($^{\emptyset 2} R^2$)

\min_{ξ}	$-3\xi_1 - 8\xi_2$			I
s.t.	$\begin{cases} \xi_1 + \xi_2 \\ 5\xi_1 - 4\xi_2 \\ -8\xi_1 + 22\xi_2 \\ -4\xi_1 - \xi_2 \\ -\xi_1 \\ -\xi_2 \end{cases}$	ママママ	$13 + x_1$ 20 $121 + x_2$ -8 0 0	



$$\xi(x) = \begin{cases} \begin{bmatrix} 0.00 & 0.05 \\ 0 & 0.06 \end{bmatrix} x + \begin{bmatrix} 11.85 \\ 9.80 \end{bmatrix} & \text{if} & \begin{bmatrix} 0.02 & 0.00 \\ 0.00 & 0.02 \\ -0.12 & 0.01 \end{bmatrix} x \le \begin{bmatrix} 1.00 \\ 1.00 \\ -1.00 \end{bmatrix} & \text{CR}_{\{2,3\}} \\ \begin{bmatrix} 0.73 & -0.03 \\ 0.27 & 0.03 \end{bmatrix} x + \begin{bmatrix} 5.50 \\ 7.50 \end{bmatrix} & \text{if} & \begin{bmatrix} 0.00 & 0.02 \\ 0.00 & -0.02 \\ 0.12 & -0.01 \\ -0.15 & 0.00 \end{bmatrix} x \le \begin{bmatrix} 1.00 \\ 1.00 \\ 1.00 \end{bmatrix} & \text{CR}_{\{1,3\}} \\ \begin{bmatrix} -0.33 & 0.00 \\ 1.33 & 0 \end{bmatrix} x + \begin{bmatrix} -1.67 \\ 14.67 \end{bmatrix} & \text{if} & \begin{bmatrix} 0.00 & 0.02 \\ 0.00 & -0.02 \\ 0.15 & -0.00 \\ -0.09 & 0.00 \end{bmatrix} x \le \begin{bmatrix} 1.00 \\ 1.00 \\ -1.00 \\ 1.00 \end{bmatrix} & \text{CR}_{\{1,4\}} \end{cases}$$

MPC for Linear Systems

Linear model

Quadratic performance index $\min_{U} J(x(t), U) = \sum_{k=0}^{N-1} \left[x'_k Q x_k + u'_k R u_k \right] + x'_N P x_N$

 $\begin{array}{ll} \text{Constraints} & \left\{ \begin{array}{l} u_{\min} \leq u_k \leq u_{\max} \\ y_{\min} \leq y_k \leq y_{\max} \end{array} \right. \end{array}$

Objective: solve the QP for all $x(t) \in X \subseteq \mathbb{R}^n$ (o-line)

Properties of multiparametric-QP

(Bemporad et al., 2002)

Optimizer	$U^*(x) = \arg \min_U \frac{1}{2}U'HU + x'F'U$ subj. to $GU \leq W + Sx$	continuous, piecewise ane
Value function	$V^*(x) = \frac{1}{2}x'Yx + \min_U \frac{1}{2}U'HU + x'F'U$ subj. to $GU \le W + Sx$	convex continuous, piecewise quadratic, C ¹ (if no degeneracy)
Feasible state set	$X^* = \{x : \exists U \text{ such that } Gx \leq W + SU\}$	convex polyhedral

Corollary: The linear MPC controller is a continuous piecewise ane function of the state

$$u(x) = \begin{cases} F_1 x + g_1 & \text{if } H_1 x \leq K_1 \\ \vdots & \vdots \\ F_M x + g_M & \text{if } H_M x \leq K_M \end{cases}$$



Polyhedral Invariant Sets for Closed-loop Linear MPC Systems

- Convexity of value function implies convexity of the piecewise ellipsoidal sets $\{x : V^*(x) \le \gamma\}$ and $\{x : V^*(x) - x'Qx \le \gamma\}$
- Any polyhedron P contained in between is a positively invariant set for the closed-loop MPC system



 By changing γ invariant polyhedra of arbitrary size can be constructed for the closed-loop MPC system

(Alessio, Bemporad, Lazar, Heemels, CDC'06)

(Note: explicit form of MPC not required)

Explicit Hybrid MPC (PWA)

$$\begin{split} \min_{U} J(U, x, r) &= \sum_{k=0}^{T-1} \|R(y(k) - r)\|_{p} + \|Qu(k)\|_{p} \\ \text{subject to} \begin{cases} \mathsf{PWA \ model} \\ x(0) &= x \end{cases} & \begin{aligned} \|v\|_{2} &= v'v \\ \|v\|_{\infty} &= \max|v_{i}| \\ \|v\|_{1} &= \sum v_{i} \end{cases} \end{split}$$

• The MPC controller is piecewise ane in x,r

$$u(x,r) = \begin{cases} F_1 x + E_1 r + g_1 & \text{if } H_1[\frac{x}{r}] \le K_1 \\ \vdots & \vdots \\ F_M x + E_M r + g_M & \text{if } H_M[\frac{x}{r}] \le K_M \end{cases}$$

(x,r)-space



(Borrelli, Baotic, Bemporad, Morari, *Automatica*, 2005) (Mayne, ECC 2001) (Alessio, Bemporad, ADHS 2006)

<u>Note</u>: in the 2-norm case the partition may not be fully polyhedral



Hybrid Control - Example

PWA system:

$$\begin{aligned} x(t+1) &= 0.8 \begin{bmatrix} \cos \alpha(t) & -\sin \alpha(t) \\ \sin \alpha(t) & \cos \alpha(t) \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t) \\ y(t) &= x_2(t) \\ \alpha(t) &= \begin{cases} \frac{\pi}{3} & \text{if } x_1(t) \ge 0 \\ -\frac{\pi}{3} & \text{if } x_1(t) < 0 \end{cases} \end{aligned}$$

Constraints: $-1 \le u(t) \le 1$

Objective: $\min \sum_{k=1}^{2} |y(t+k|t) - r(t)|$

Open loop behavior:



Closed loop:



60

ime offset: 0

HybTbx: /demos/hybrid/bm99sim.m

Explicit PWA Controller



(CPU time: 1.51 s, Pentium M 1.4GHz)

Hybrid MPC - Example

Closed loop:



Explicit PWA Regulator

Objective: $\min \sum_{k=1}^{N} ||x(t+k|t)||_{\infty}$



HybTbx: /demos/hybrid/bm99benchmark.m

Comments on Explicit Solutions

- Alternatives: either (1) solve an MIP on-line or (2) evaluate a PWA function
- For problems with many variables and/or long horizons: MIP may be preferable
- For simple problems (short horizon/few constraints):
 - time to evaluate the control law is shorter than MIP
 - control code is simpler (no complex solver must be included in the control software !)
 - more insight in controller's behavior

Contents

- ✓ Models of hybrid systems
- \checkmark Model predictive control of hybrid systems
- ✓ Explicit reformulation
- Automotive applications



(Photo: Courtesy Mitsubishi)

Hybrid Control of a DISC Engine

(joint work with N. Giorgetti, G. Ripaccioli, I. Kolmanovsky, and D. Hrovat)



DISC Engine



Objective: Design a controller for the engine that

- Automatically choose operating **mode** (homogeneous/stratied)
- Can cope with **nonlinear** dynamics
- Handles constraints (on A/F ratio, air-ow, spark)
- Achieves **optimal** performance

Hybridization of DISC Dynamics

- Proprietary nonlinear model of the DISC engine developed and validated at Ford Research Labs (Dearborn) (Kolmanovsky, Sun, ...)
- Model good for simulation, not good for control design!

MODEL HYBRIDIZATION

<u>DYNAMICS</u> (intake pressure, air-to-fuel ratio, torque):

- Denition of two operating points;
- Numerical linearization of nonlinear dynamics;
- Time discretization of the linear models.

CONSTRAINTS on:

- Air-to-Fuel Ratio: $\lambda_{min}(\rho) \leq \lambda(t) \leq \lambda_{max}(\rho);$
- Mass of air through the throttle: $0 \le W_{th} \le K$;
- Spark timing: $0 \leq \delta(t) \leq \delta_{mbt}(\lambda, \rho)$

Hybrid system with 2 modes (switched ane system)

p-dependent dynamic
equations



 ρ -dependent constraints

46

Integral Action

Integrators on torque error and air-to-fuel ratio error added to obtain zero osets in steady-state:

$$\epsilon_{\tau}(t+1) = \epsilon_{\tau}(t) + T \cdot (\tau_{ref} - \tau)$$

$$\epsilon_{\lambda}(t+1) = \epsilon_{\lambda}(t) + T \cdot (\lambda_{ref} - \lambda)$$

T =sampling time

 au_{ref} , λ_{ref} brake torque and air-to-fuel references

Simulation based on nonlinear model conrms zero osets in steady-state

(despite the model mismatch)

Reference values are automatically generated from τ_{ref} and λ_{ref} by numerical computation based on the nonlinear model

DISC Engine - HYSDEL List

```
SYSTEM hysdisc{
  INTERFACE {
  STATE {
               [1, 101.325];
    REAL pm
    REAL xtau [-1e3, 1e3];
    REAL xlam [-1e3, 1e3];
    REAL taud [0, 100];
    REAL lamd
              [10, 60];
     }
  OUTPUT {
    REAL lambda, tau, ddelta;
  INPUT {
    REAL Wth
                [0,38.5218];
    REAL Wf
               [0, 2];
    REAL delta [0,
                        401;
    BOOL rho;
    }
   PARAMETER {
    REAL Ts, pm1, pm2;
    ...
  IMPLEMENTATION {
  AUX {
    REAL lam, taul, dmbtl, lmin, lmax;
     }
  DA {
  lam={IF rho THEN ll1*pm+ll2*Wth...
              +113*Wf+114*delta+11c
       ELSE 101*pm+102*Wth+103*Wf...
              +104*delta+10c
                              };
```

```
taul={IF rho THEN taul1*pm+...
  tau12*Wth+tau13*Wf+tau14*delta+tau1c
      ELSE tau01*pm+tau02*Wth...
      +tau03*Wf+tau04*delta+tau0c };
dmbtl ={IF rho THEN dmbt11*pm+dmbt12*Wth...
        +dmbt13*Wf+dmbt14*delta+dmbt1c+7
        ELSE dmbt01*pm+dmbt02*Wth...
        +dmbt03*Wf+dmbt04*delta+dmbt0c-1};
lmin ={IF rho THEN 13 ELSE 19};
lmax ={IF rho THEN 21 ELSE 38};
CONTINUOUS {
    pm=pm1*pm+pm2*Wth;
    xtau=xtau+Ts*(taud-taul);
    xlam=xlam+Ts*(lamd-lam);
    taud=taud; lamd=lamd;
OUTPUT {
   lambda=lam-lamd;
   tau=taul-taud;
   ddelta=dmbtl-delta:
MUST {
   lmin-lam
              <=0;
   lam-lmax
              <=0;
   delta-dmbtl <=0;
```

MPC of DISC Engine

$$\begin{split} \min_{\xi} J(\xi, x(t)) &= \sum_{k=0}^{N-1} u_k' R u_k + y_k' Q y_k + x_{k+1}' S x_{k+1} \\ \text{subj. to} & \begin{cases} x_0 = x(t), \\ \text{hybrid model} \end{cases} \end{split}$$

 $u(t) = [W_{th}(t), W_f(t), \delta(t), \rho(t)]$

Weights:



Solve MIQP problem (mixed-integer quadratic program) to compute u(t)



Simulation Results (nominal engine speed)



Simulation Results (varying engine speed)





20 s segment of the European drive cycle (NEDC)

Hybrid MPC design is quite robust with respect to engine speed variations

Control code too complex (MILP) \Rightarrow not implementable !

Explicit MPC Controller



Microcontroller Implementation

- C-code automatically generated by the Hybrid Toolbox
- Microcontroller Motorola MPC 555 (custom made for Ford)
- 43 Kb memory available
- Floating point arithmetic





sampling period = 10ms





• Further reduction of number of partitions possible

(Alessio, Bemporad, 2005)

• C-code can be further optimized

(Tøndel, Johansen, Bemporad, 2003)

Conclusions

- Hybrid systems as a framework for new applications, where both logic and continuous dynamics are relevant
- Supervisory MPC controllers schemes can be synthesized via on-line mixed-integer programming (MILP/MIQP)
- Piecewise Linear MPC Controllers can be synthesized o-line via multiparametric programming for fast-sampling applications



Hybrid MPC & Wireless Sensor Networks



- Measurements acquired and sent to base station (MPC) by wireless sensors
- MPC computes the optimal plan when new measurements arrive
- Optimal plan implemented by local controller if received in time, otherwise previous plan still kept

Packet loss possible along both network links, delayed packets must be discarded (out-of-date data)

Challenges in Wireless MPC





 Synchronization schemes must ensure correct prediction in spite of packet loss

● MPC algorithm must be robust w.r.t. packet loss
 ⇒ stochastic hybrid MPC, robust hybrid MPC

Wireless sensors must be interfaced to optimization tools

Demo Application in Wireless Automation



(Bemporad, Di Cairano, Henriksson)

Telos motes



(Automatic Control Lab, Univ. Siena)

- Telos motes provide wireless temperature feedback in Matlab
- Hybrid MPC algorithm adjust belt speed and coordinate linear motors (via Simulink/xPC-Target link)



Acknowledgements

A. Alessio, M. Baotic, F. Borrelli, B. De Schutter,
S. Di Cairano, G. Ferrari-Trecate, K. Fukuda, N. Giorgetti,
M. Heemels, D. Hrovat, J. Julvez, I. Kolmanovski, M. Lazar,
L. Ljung, D. Mignone, M. Morari, D. Munoz de la Pena,
S. Paoletti, G. Ripaccioli, J. Roll, F.D. Torrisi

Announcements

- 10th "Hybrid Systems: Computation and Control" Conference (Pisa, Italy, April 3-5, 2006). **Submission: Oct. 9, 2006**
- 2nd PhD School on Hybrid Systems, Siena, 2007



The End

MPC controller - SIMO DC-Servomotor Hybrid Toolbox

http://www.dii.unisi.it/hybrid/toolbox