



www.unisi.it

1st HYCON PhD School on Hybrid Systems



www.ist-hycon.org

Hybrid Systems in Industrial Process Control

Olaf Stursberg

University of Dortmund, Germany

o.stursberg@ct.uni-dortmund.de



HYSCOM

IEEE CSS Technical Committee on Hybrid Systems



Information Society Technologies

Siena, July 19-22, 2005 - Rectorate of the University of Siena



Hybrid Systems in Industrial Process Control

Olaf Stursberg

Process Control Laboratory
University of Dortmund, Germany

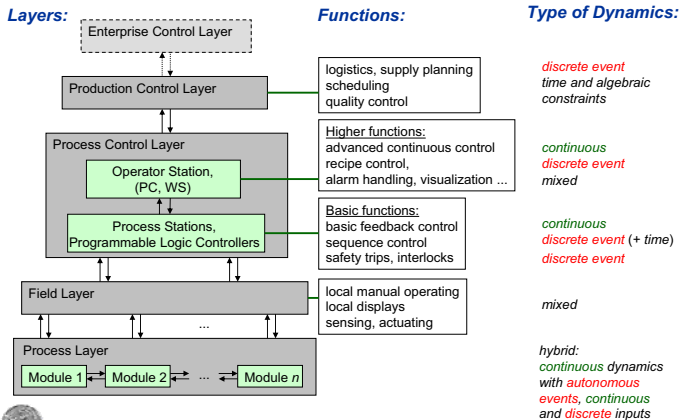


Outline

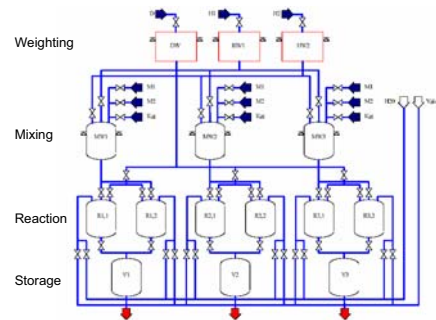
- Control Architecture of Production Systems
- Design Tasks
- Modeling with Hybrid Automata
- Optimal Control of Transition Procedures
- Synthesis of Supervisory Controllers
- Controller Verification using Reachability Analysis
- Conclusions and Open Problems



Control Structure of Production Systems



Example: Polymer Production Plant



- Controller Functions:**
- (1) **Coordination control:**
- follow recipes
- assign task to resources
[mostly DCS, operator]
 - (2) **Group control:**
supervise the sequence of control actions in one unit [PLC + Industrial PC]
 - (3) **Basic Control:**
supervise / control one (or a few) dependent process quantities [mostly PLC, hard-wired; feedback loops]



Design Task

Control design for production plants ...

- ... is challenging:
- **heterogeneity:** the various control functions require different models and design techniques
 - **interdependency:** functions on different layers affect each other; *how to guarantee consistency?*
 - **complexity:** – due to dynamic type (nonlinearity, non-convexity)
– due to size (large number of state variables, manipulated variables, operating modes, etc.)
– hardware requirements
 - **modularity:** *suitable communication paradigms?*

... includes the following tasks:

- optimization of transition procedures → **optimal control**
- algorithmic generation of supervisory controllers → **synthesis**
- a-posteriori analysis of the control design → **verification**

What can hybrid systems contribute?



Modeling with Hybrid Automata – Syntax

Hybrid automaton: $HA = (X, U, V, Z, inv, \theta, g, r, f)$

- continuous states: $x \in X \subseteq R^{n_x}$
- continuous inputs: $u \in U = [u_1^-, u_1^+] \times \dots \times [u_{n_u}^-, u_{n_u}^+]$
- finite set of discrete inputs: $v \in V = \{v_1, \dots, v_{n_d}\}, v_j \in R^{n_{v_j}}$
- finite set of locations: $Z = \{z_1, \dots, z_{n_z}\}$
- invariants: $inv : Z \rightarrow 2^X$, polyhedral for all z
- transitions: $(z_1, z_2) \in \theta \subseteq Z \times Z$
- guards: $g : \theta \rightarrow 2^X$, polyhedral
- resets: $r : \theta \times X \rightarrow X$
- flow functions: $f : Z \times X \times U \times V \rightarrow R^{n_x}$
s.t. $\dot{x} = f(z, x, u, v)$ defines a continuous vector field

[for simplicity: no synchronization]



Modeling with Hybrid Automata – Semantics

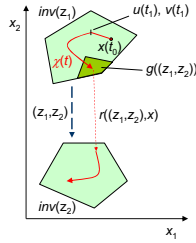
Set of event times: $T = \{t_0, t_1, t_2, \dots\}$

Input trajectories: $\phi_u = (u_0, u_1, \dots) \in \Phi_u$,
 $\phi_v = (v_0, v_1, \dots) \in \Phi_v$
 with u_k, v_k constant for $t \in [t_k, t_{k+1}[$

Hybrid state: $\sigma_k \in (z_k, x_k) \in \Sigma$ with
 $x_k = x(t_k), z_k = z(t_k)$

Feasible run of HA for given σ_0, ϕ_u and ϕ_v :
 $\phi_\sigma = (\sigma_0, \sigma_1, \sigma_2, \dots)$ with σ_k from:

- (i) continuous evolution: $\chi(0) = x_k$ and $\chi(t)$ is the unique solution of the flow function for $t \in [0, \tau]$; $\chi(t) \in \text{inv}(z_k)$ but $\chi(t) \notin g(z_k, \bullet)$ for $t < \tau$
- (ii) transition: $(z_k, z_{k+1}) \in \Theta$, $\chi(\tau) \in g(z_k, z_{k+1})$, and
 $x_{k+1} = f(z_k, z_{k+1}, \chi(\tau)) \in \text{inv}(z_{k+1})$

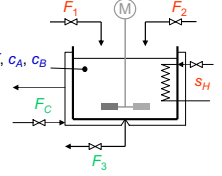
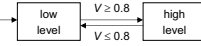


Modeling with Hybrid Automata – Example

Reactor with liquid-phase chemical reaction:

Variables: • discrete inputs: F_1, F_2, S_H
 • continuous inputs: F_C, F_3
 • state variables: V, T, c_A, c_B

Discrete dynamics: (no resets)



Continuous dynamics: $\frac{dV}{dt} = F_1 + F_2 - F_3$

$$\frac{dT}{dt} = \frac{F_1(k_1 - T) + F_2(k_2 - T) + F_C k_3(k_4 - T) f_{v,1} + k_5 f_r + s_h k_6(k_7 - T) f_{v,2}}{V}$$

$$\frac{dc_A}{dt} = \frac{F_1(k_8 - c_A) - F_2 c_A + k_9 f_r}{V}$$

$$\frac{dc_B}{dt} = \frac{F_1(k_{10} - c_B) - F_2 c_B + k_{11} f_r}{V}$$

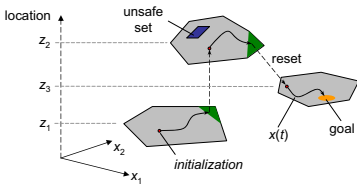
$$\text{with: } f_{v,1} = k_{12} + \frac{k_{13}}{V}, \quad f_{v,2} = k_{14} - \frac{k_{15}}{V}, \quad f_r = c_A c_B^2 \exp\left(\frac{-k_{16}}{T}\right)$$

only for "high level"

Task 1: Optimal Control of Transition Procedures

- given: • hybrid automaton
 • specifications: → transfer from initial state to goal set
 → safety restriction (exclusion of unsafe states)
 → maximized performance / minimized costs

[industrial relevance: start-up, shut-down, or change-over of processing systems]



Objective:
 Determine input trajectories
 such that the specs are met!

Literature:
 different approaches suggested; most based on piecewise affine approximations

Problem Statement

Target region: $(z_{tar}, x_{tar}) \in \Sigma_{tar} \subset \Sigma$, with one $z_{tar} \in Z$, $x_{tar} \in \text{inv}(z_{tar})$

Forbidden sets: $F = \{F_1, \dots, F_{n_f}\}$ with $F_j \subset \Sigma$, polyhedral continuous sets

Assume: time set $T = \{t_0, t_1, \dots, t_f\}$ is finite

Optimal control task:

determine ϕ_u^*, ϕ_v^* such that ϕ_σ^* is the solution to:

$$\min_{\phi_u \in \Phi_u, \phi_v \in \Phi_v} \Omega(t_f, \phi_u, \phi_v, \phi_\sigma)$$

subject to: • $\phi_\sigma \in \Phi_\sigma$ (set of feasible runs)
 • $\sigma_0 = (z_0, x_0)$, $\sigma_f \in \Sigma_{tar}$, $\sigma \notin F$

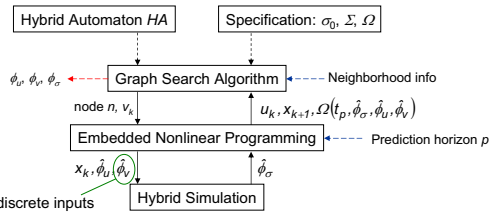
Chosen cost function Ω :

t_f in combination with weighted distances of σ_k to Σ_{tar}

Decomposition Approach

Principle:

- separate the optimization of continuous and discrete degrees of freedom:
 - (i) high level: search tree encoding the discrete DOF → $v(t)$
 - (ii) low level: embedded NLP for the continuous DOF → $u(t)$
- branch&bound and heuristics to prune the search tree efficiently
- cost function evaluated by hybrid simulation



Results for the Example (1)

- Objectives: • reach nominal reaction (target) from an initially empty reactor
 • time optimality
 • avoid overflow and critical temperatures

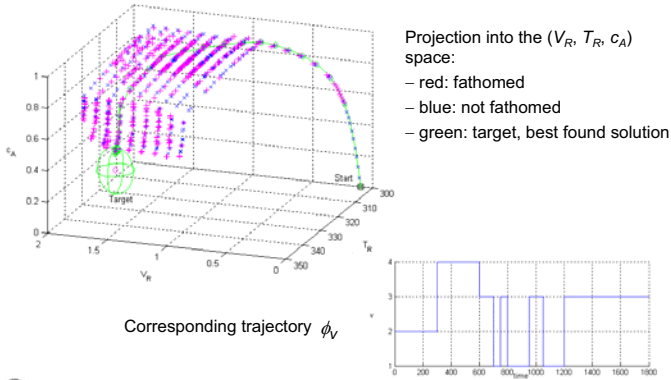
Configurations:

- best-first search (throughout)
- pruning based on an adjacency criterion (chooses a locally best v_k)
- prediction horizon: $p = 2$

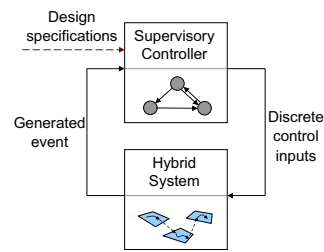
Results:

- termination after 959 nodes,
- 721 nodes fathomed due to adjacency, the remainder due to costs [theoretical number of nodes for the encountered path length: $3 \cdot 10^{14}$]
- computation time: 484 CPU-sec (P4-1.5 GHz)

Results for the Example (2)



Task 2: Synthesis of Supervisory Controllers



given:

(1) hybrid automaton HA :

- no continuous inputs
- discrete inputs: degree of freedom
- continuous controllers (if any) are embedded in the continuous dynamics
- generates events if transitions occur

(2) design specifications:

- goal attainment: reach target set from initial set
- safety: always avoid critical sets

Objective: determine a supervisory controller as finite automaton

- selects discrete control inputs upon receiving events
- here: no delay of the controller response

Synthesis Problem

Modified semantics of HA :

- if $x(t)$ enters a guard g , the transition must be taken before g is left
- the discrete input v can be changed only when a transition is taken

Given Sets:

- initial set of hybrid states: $(z_0, x_0) \in \Sigma_0$ with $z_0 \in Z, x_0 \in \text{inv}(z_0)$
- forbidden sets of hybrid states: $\Sigma_F = \{\Sigma_{F1}, \dots, \Sigma_{Fp}\}$
- hybrid goal set: $(z_G, x_G) \in \Sigma_G$ with $z_G \in Z, x_G \in \text{inv}(z_G)$

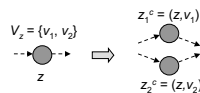
Synthesis Problem:

compute an input sequence (v_0, v_1, v_2, \dots) such that any $(z_0, x_0) \in \Sigma_0$ is driven into Σ_G by a feasible run that never encounters any hybrid state in Σ_F .

First Step:

rewrite HA into a closed system HA^c :

consider that any $v \in V_z$ can be applied in $z \in Z$

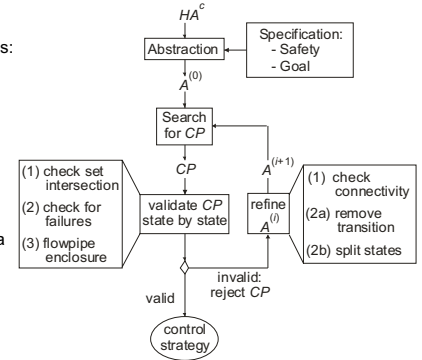


Solution based on Abstraction Refinement

Principle:

- use an **abstract model** to identify promising evolutions: *candidate paths CP*
 - **validate CP** for the original model with lowest possible computational effort
 - if necessary: **refine** the abstract model for the next iteration
- a validated *CP* represents a proper control strategy

[similar to counterexample-guided verification of HA^c , see below]



Abstraction and Candidate Paths

Abstract Model: represents the discrete dynamics of HA^c

Finite state automaton: $A^{(0)} = (\hat{S}, \hat{S}_0, \hat{E})$

Abstraction function: $\alpha: Z^c \times X \rightarrow \hat{S}$ such that:

- states: - one state \hat{s} for any location z^c
- separate states for the sets: $\hat{S}_0, \hat{S}_G, \hat{S}_F$
- transitions: \hat{E} according to the set Θ^c

Run of $A^{(0)}$: $(\hat{s}_0, \hat{s}_1, \hat{s}_2, \dots)$

Candidate Path: $CP = (\hat{s}_0, \hat{s}_1, \dots, \hat{s}_p)$ with $\hat{s}_0 \in \hat{S}_0, \hat{s}_p \in \hat{S}_G$ and $\hat{s}_k \notin \hat{S}_F$ for all $k \in \{0, \dots, p\}$

Search for *CP*: standard forward breadth-first algorithm

→ returns one of the shortest candidate paths existing for $A^{(0)}$

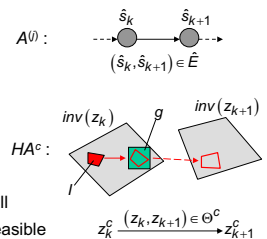
Validation

Check for any pair $(\hat{s}_k, \hat{s}_{k+1})$ of *CP* whether it realizes a feasible control action for HA^c :

$I \subset \text{inv}(z_k^c)$ - set of continuous states represented by \hat{s}_k

⇒ any state $x \in I$ must be transferred into $\text{inv}(z_{k+1}^c)$ by:

- continuous evolution
- transition and reset



Validation procedure: determine with an as small effort as possible that the control action is **not** feasible

- (1) intersection check
- (2) search for invalidating trajectories
- (3) flowpipe enclosure

↓ *stricter condition, higher computational effort*
 [details: Stursberg et al. 2005]

Refinement

$A^{(i)}$ is refined to $A^{(i+1)}$ in the following cases:

- (1) if the intersection check shows that $(z_k^c, z_{k+1}^c) \in \Theta^c$ can never be taken, the corresponding transition $(\hat{s}_k, \hat{s}_{k+1})$ is removed from \hat{E} .
- (2) if the other two validation methods show that $(\hat{s}_k, \hat{s}_{k+1})$ is invalid, it cannot be removed from \hat{E} immediately.
[Krogh et al., 2003: optimization-based method to show that $(z_k^c, z_{k+1}^c) \in \Theta^c$ cannot occur]
- (3) if flowpipe approximation validates a control action, state splitting can be used optionally:
 - new abstract state for the reachable subset of $inv(z_{k+1}^c)$
 - transition set \hat{E} modified according to the reachability result
 - can be advantageous to (in-)validate a CP computed later



Application: Reactor Example (1)

Continuous chemical liquid-phase reactor:

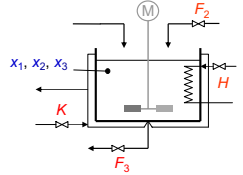
modified setting:

- state variables: x_1 (level), x_2 (temperature), x_3 (concentration)
- inputs: F_2 (flow), F_3 (flow), K (cooling), H (heating)
- 16 possible combinations of discrete values
- hybrid automaton:
 - 12 locations (32 for HA^c), 22 transitions
 - dynamics for $x_1 < 0.8$:

$$\dot{x}_1 = k_1 + F_2 + F_3, \dot{x}_2 = \frac{k_2(k_3 - x_2) + F_2(k_4 - x_2)}{x_1} + k_5K(k_6 - x_2) \left(\frac{k_7}{x_1} + k_8 \right), \dot{x}_3 = (k_9 - (k_{10} + F_2)x_3) / x_1$$
 - for $x_1 \geq 0.8$:

$$\dot{x}'_2 = x_2 + k_{11}(k_{12} - x_2)(k_{13} - k_{14} / x_1)H$$
 - for $(0, k_{15}, k_{16}) \cdot x \geq k_{17}$:

$$x''_2 = x'_2 + x_3(k_{18} + k_{19}x_2^2), \dot{x}'_3 = \dot{x}_3 + k_{20} \cdot \exp(k_{21} / x_2)$$



Application: Reactor Example (2)

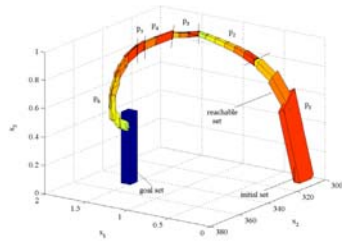
Task: find a control strategy for start-up into nominal operation
initially: reactor empty, goal state: high level, temperature, and yield

Control synthesis:

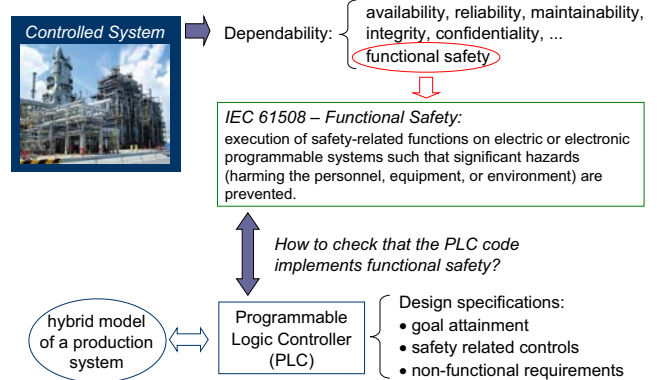
- 17th CP: feasible strategy
- six phases p_1 to p_6 :

V_{p1}	V_{p6}
1	0
0	1
0	0
0	0
0	1
- 16 CP invalidated by the 2nd validation method
- obtained in approx. 4 minutes on a standard PC (P4-1.5GHz)

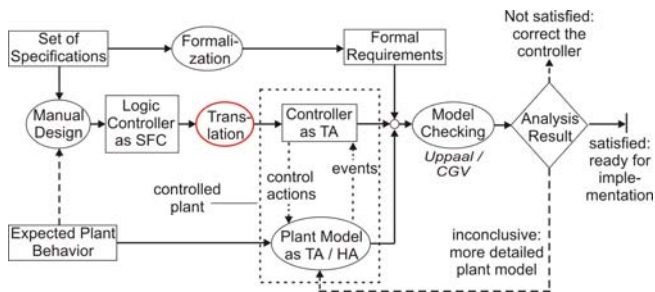
reachable set for the control strategy:



Task 3: Verification of Logic Controllers



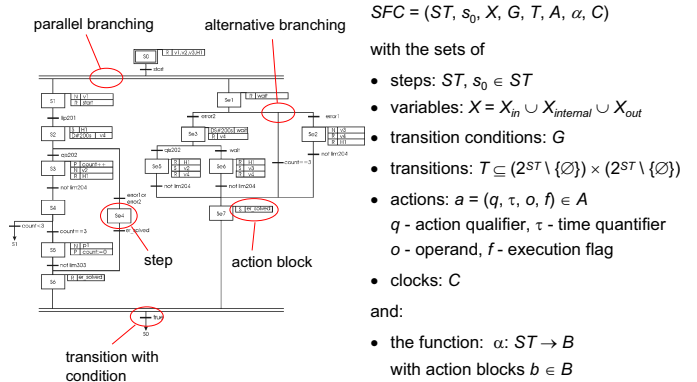
Verification Approach



SFC: Sequential Function Charts (standardized language for logic controllers)
TA: Timed Automata
CGV: Matlab tool for counterexample-guided verification



Sequential Function Charts



Application: Verification with Uppaal

- **Parallel composition** of all controller and plant automata; two additional automata to model malfunctions of the heater and the cooling
- **Formal requirements:**
 - (1) E \leftrightarrow tank2.emptying (production goal can be reached)
 - (2) A [] not liquid.crystallizing (if heater malfunction, temp. in T1 not too low)
 - (3) A [] not liquid.overpressure (if cooling malfunction, temp. in T1 not too high)
- **Verification:**
 - model checking with *Uppaal* [Larsen et al., 2000]
 - standard PC (Pentium 1.5 GHz)
- **Results:**
 - no deadlock, state 'tank2.emptying' eventually always reached (nominal production realized)
 - 2nd and 3rd property satisfied \Rightarrow **functional safety achieved**
 - computation time: below 1 second in all cases



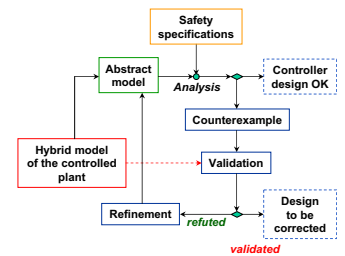
Application: Verification with CGV (1)

Hybrid Model:

- State variables: x_1 (temperature in T1), x_2 (level in T1), x_3 (level in T2)
- Nonlinear ODEs for the combinations of the following cases:
 - levels x_2 and x_3 : *filling, emptying, constant*; for x_2 in addition: *evaporating*
 - temperature x_1 : *heating, heat loss to environment*

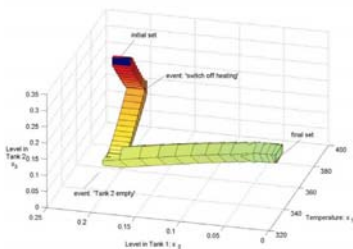
Verification with CGV:

- Abstractions used to identify potentially unsafe behaviors
- Hierarchy of different validation methods
 - \Rightarrow computation of reachable sets only for a 'small' part of the hybrid state space



Application: Verification with CGV (2)

computed reachable hybrid set:



- **Scenario:**
 - during evaporation (x in initial set): malfunction of the condenser
- **Task:** verify whether $x_1 > 394\text{K}$ and $x_1 < 339\text{K}$ is avoided
- Computational time: around 1 minute (P4-1.8 GHz)
- **Result:**
 - critical temperatures not reached (no overpressure, final set: T1 emptied before crystallization at $x_1 < 339\text{K}$)
 - the SFC-controller fulfills the requirements!



Conclusions and Open Problems

Status Quo:

- Hybrid models are appropriate to formulate the different dynamics occurring in industrial plants.
- First tools for optimization, control synthesis, and verification exist.
- Size of problems tractable so far: only relatively small parts of the plant, or only simple specifications.
- Robustness / model uncertainties not yet considered to a sufficient extent.

Open Problems:

- Find clever methods to handle complexity (decomposition, abstraction, ...).
- Use of stochastic models and corresponding techniques.
- Connect hybrid models to the languages used in industry.
- Make practitioners aware of design techniques based on hybrid systems. (... *modeling must be easy* ...)



References

- O. Stursberg, S. Panek, J. Till, S. Engell: Generation of Optimal Control Policies for Systems with Switched Hybrid Dynamics. In: *Modelling, Analysis, and Design of Hybrid Systems*, Springer, LNCS, Vol. 279, 2002, 337-352.
- O. Stursberg: A Graph-Search Algorithm for Optimal Control of Hybrid Systems. *43rd IEEE Conf. on Decision and Control*, 2004, 1412-1417.
- O. Stursberg: Synthesis of Supervisory Controllers for Hybrid Systems using Abstraction Refinement. *16th IFAC World Congress*, 2005, ID: We-M12-TO/2.
- E. Clarke, A. Fehnker, Z. Han, B.H. Krogh, J. Ouaknine, O. Stursberg, M. Theobald: Abstraction and Counterexample-Guided Refinement in Model Checking of Hybrid Systems. *Intern. Journal Foundations of Computer Science*, Vol. 14 (4), 2003, 583-604.
- O. Stursberg, S. Lohmann, S. Engell: Improving Dependability of Logic Controllers by Algorithmic Verification. *16th IFAC World Congress*, 2005, ID: Mo-E17.TO/6.
- O. Stursberg, B.H. Krogh: Efficient Representation and Computation of Reachable Sets for Hybrid Systems. In: *Hybrid Systems - Computation and Control*, Springer, LNCS, Vol. 2623, 2003, 482-497.
- N. Bauer, S. Engell, R. Huuck, S. Lohmann, B. Lukoschus, M.P. Remelhe, O. Stursberg: Verification of PLC Programs given as Sequential Function Charts. In: *Integration of Software Specification Techniques for Applications in Engineering*, Springer, LNCS, Vol. 3147, 2004, 517-540.

