

Optimization-Based Methods for Controller Synthesis and Verification

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<http://www.dii.unisi.it/hybrid>

“Computation and Control”

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Review Meeting

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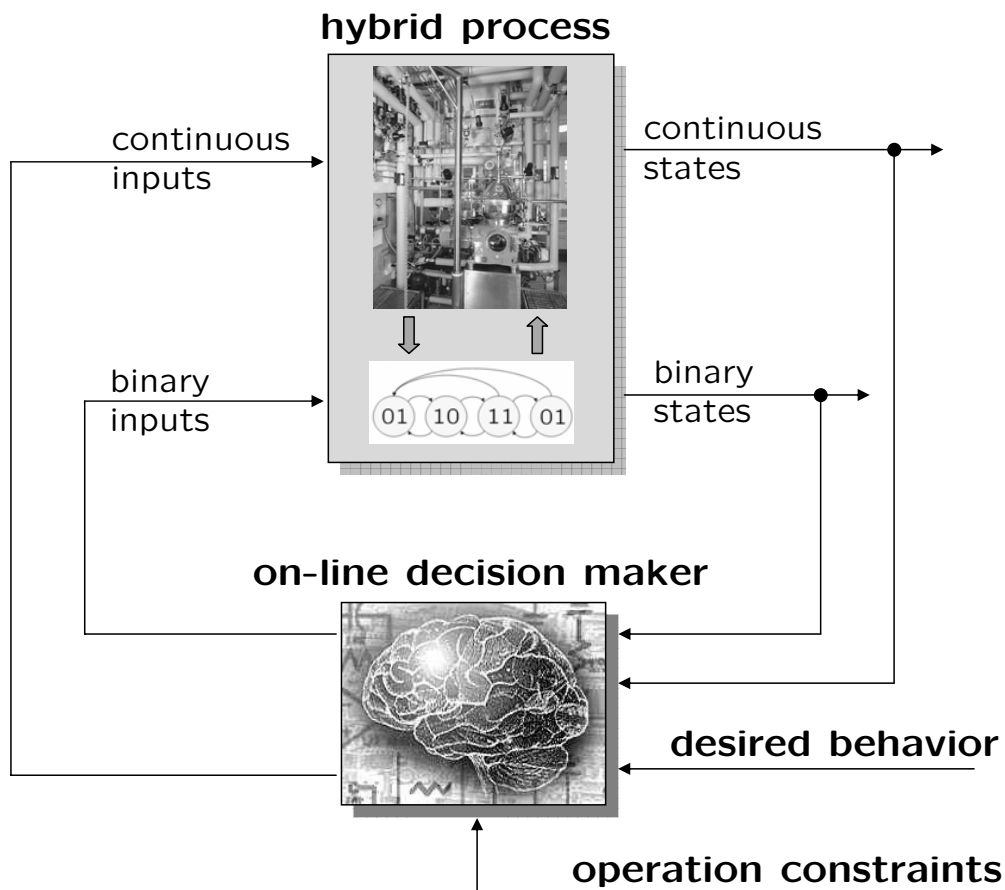
COHES Group
Control and Optimization of Hybrid and Embedded Systems

Dept. of Information
Engineering

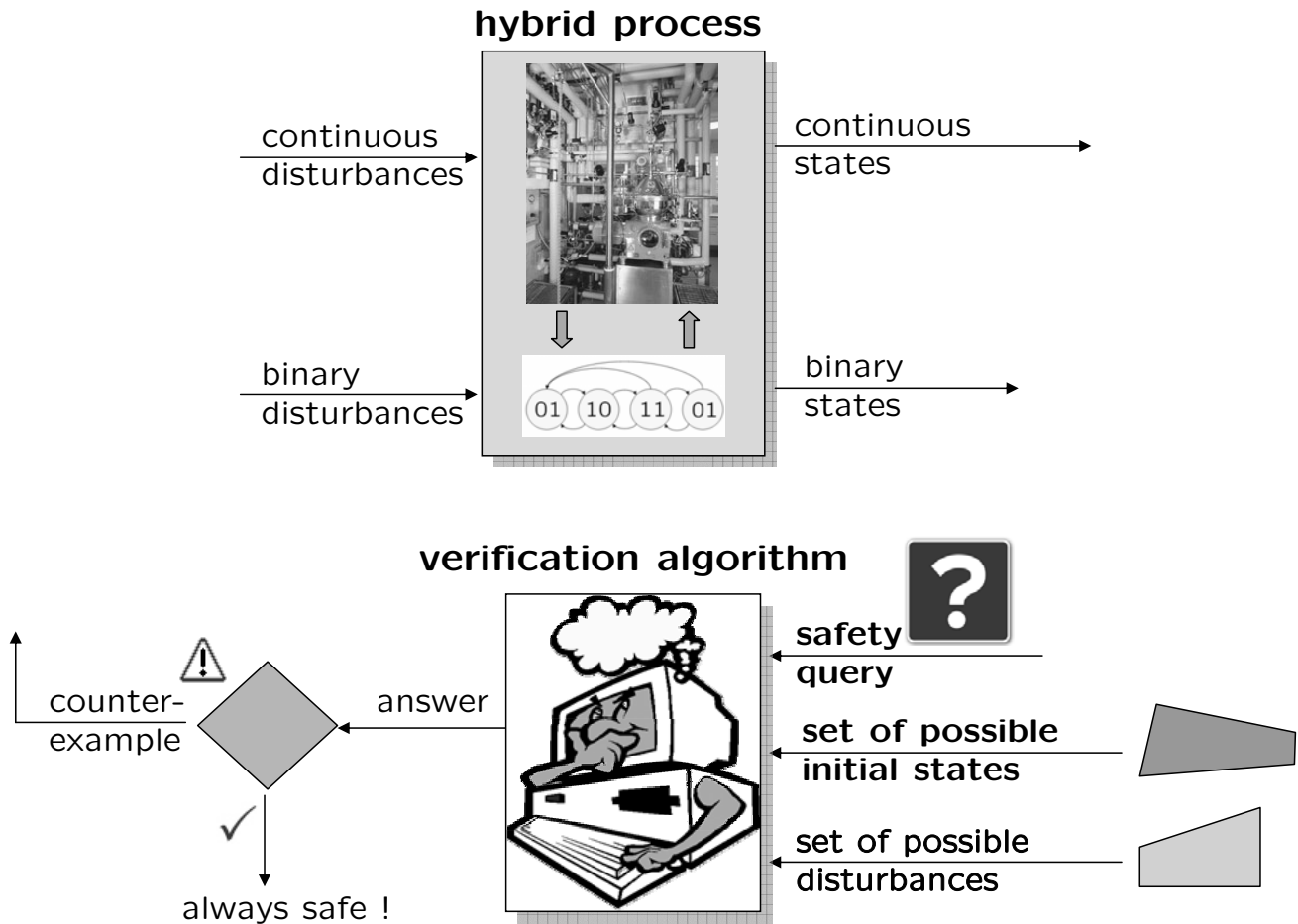
University of Siena, Italy
(founded in 1240)



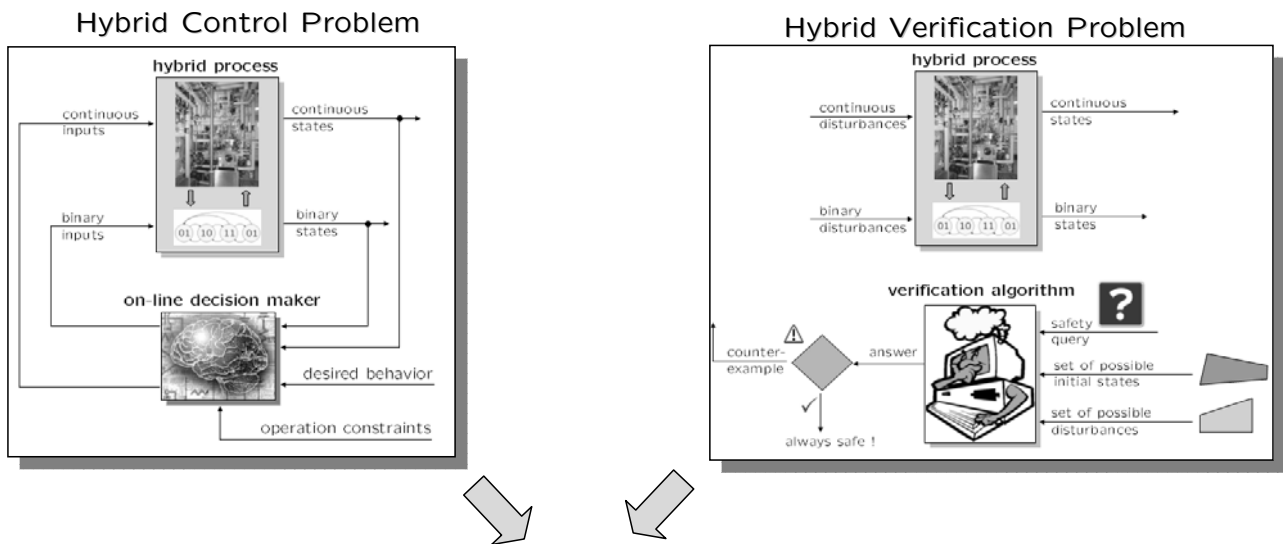
Hybrid Control Problem



Hybrid Verification Problem

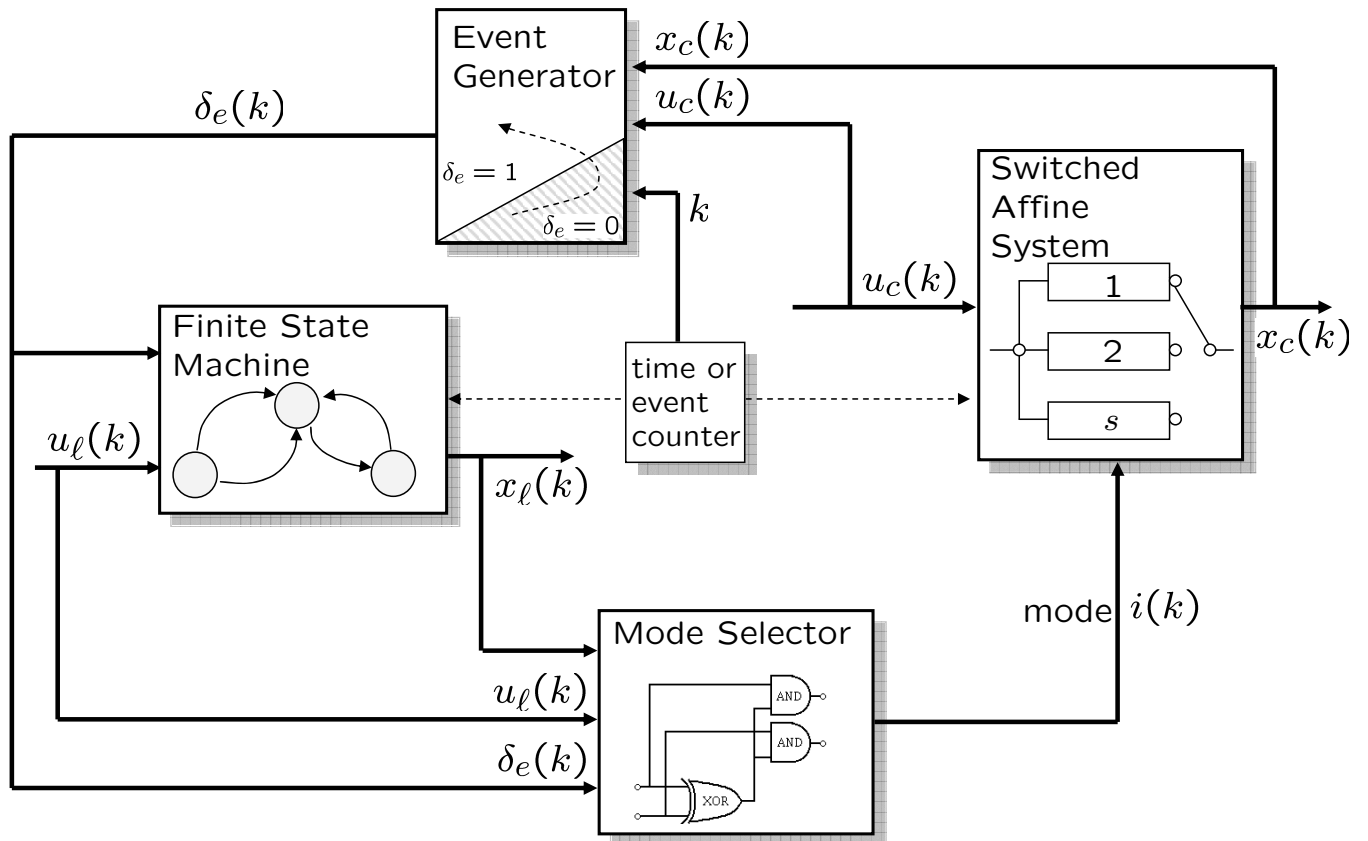


Model-based Optimization Approach



- Need for a hybrid model of the process reproducing the behavior of the process (simulation)
- A model suitable for controller synthesis and verification
- A model for which computational tools can be applied

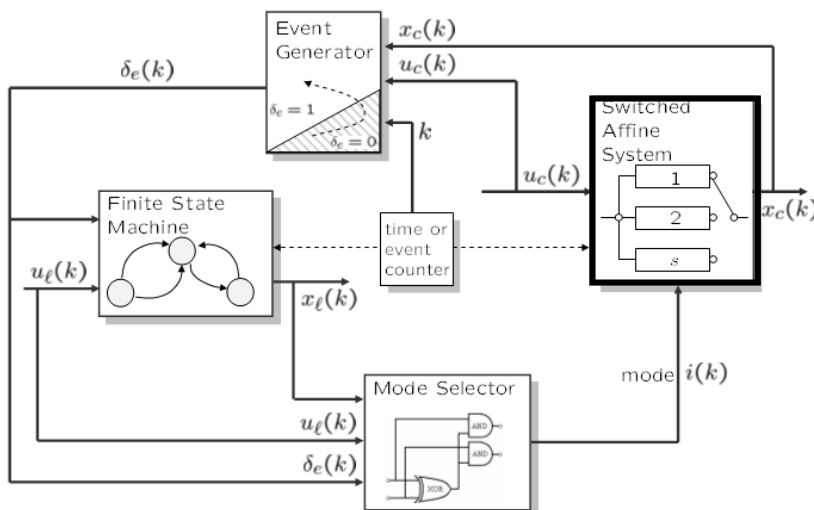
Hybrid Model: Discrete Hybrid Automaton



$x_c \in \mathbb{R}^{n_r}$ = continuous states
 $x_l \in \{0, 1\}^{n_b}$ = binary states
 $i(k) \in \{1, \dots, s\}$ = current mode

$u_c \in \mathbb{R}^{m_r}$ = continuous inputs
 $u_l \in \{0, 1\}^{m_b}$ = binary inputs
 $\delta_e \in \{0, 1\}^{n_e}$ = event conditions

Switched Affine System

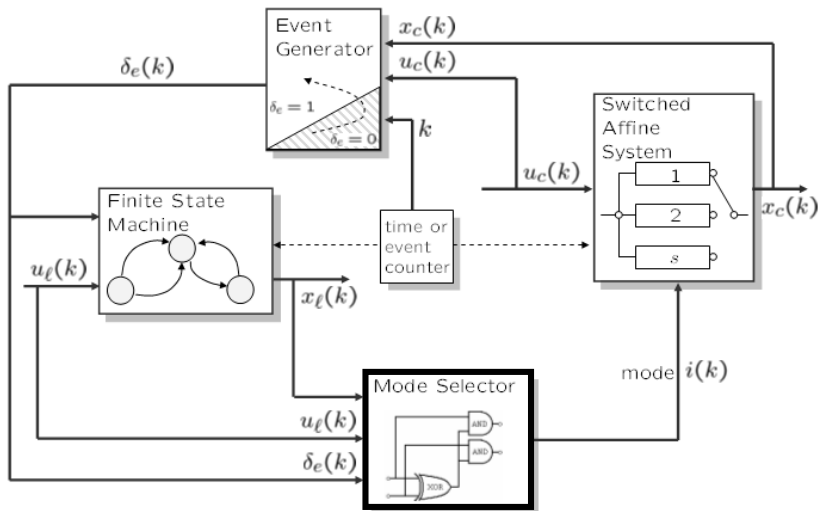


The affine dynamics depend on the current mode $i(k)$:

$$x_c(k + 1) = A_{i(k)}x_c(k) + B_{i(k)}u_c(k) + f_{i(k)}$$

$x_c \in \mathbb{R}^{n_c}$, $u_c \in \mathbb{R}^{m_c}$

Mode Selector



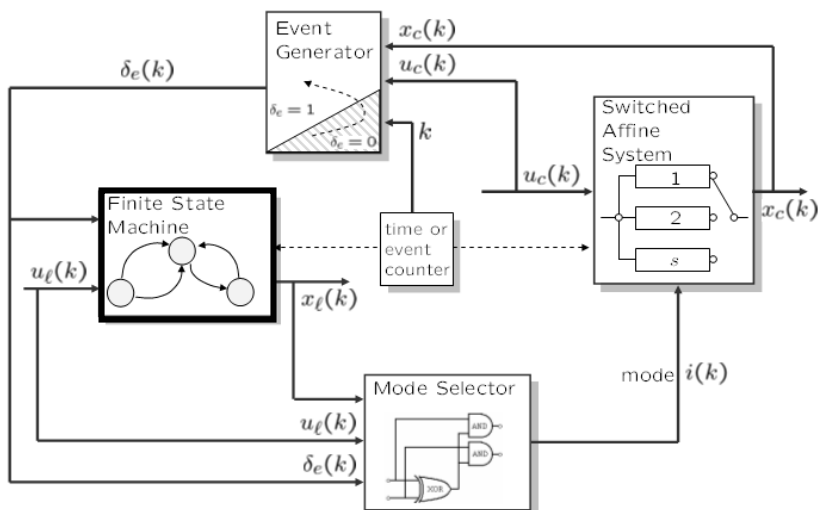
The active mode $i(k)$ is selected by a Boolean function of the current binary states, binary inputs, and event variables:

$$i(k) = f_M(x_\ell(k), u_\ell(k), \delta_e(k)) \quad x_\ell \in \{0, 1\}^{n_\ell}, u_\ell \in \{0, 1\}^{m_\ell}, \delta_e \in \{0, 1\}^{n_e}$$

Example:

$$i(k) = \begin{bmatrix} \neg u_\ell(k) \vee x_\ell(k) \\ u_\ell(k) \wedge x_\ell(k) \end{bmatrix} \Rightarrow \begin{array}{c|cc} u_\ell/x_\ell & 0 & 1 \\ \hline 0 & i = \begin{bmatrix} 1 \\ 0 \end{bmatrix} & i = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \\ \hline 1 & i = \begin{bmatrix} 0 \\ 0 \end{bmatrix} & i = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \end{array} \quad \text{the system has 3 modes}$$

Finite State Machine

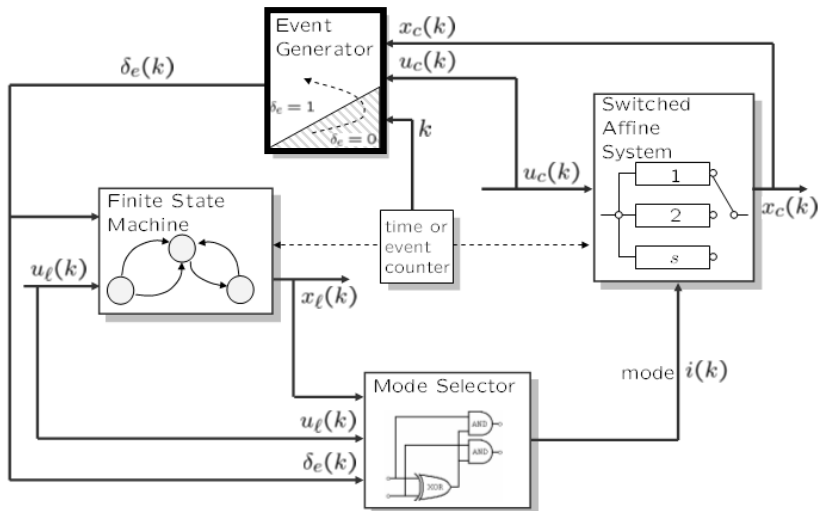


The binary state of the finite state machine evolves according to a Boolean state update function:

$$x_\ell(k+1) = f_B(x_\ell(k), u_\ell(k), \delta_e(k)) \quad x_\ell \in \{0, 1\}^{n_\ell}, u_\ell \in \{0, 1\}^{m_\ell}, \delta_e \in \{0, 1\}^{n_e}$$

Example: $x_\ell(k+1) = \neg \delta_e(k) \vee (x_\ell(k) \wedge u_\ell(k))$

Event Generator



Event variables are generated by linear threshold conditions over continuous states, continuous inputs, and time:

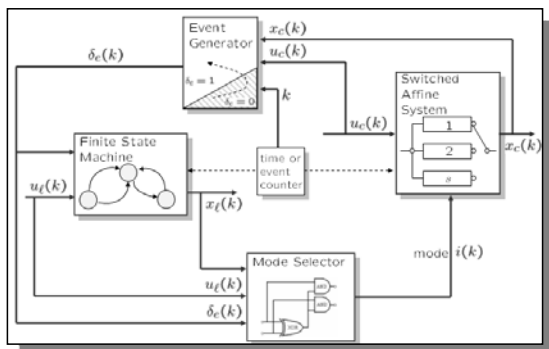
$$[\delta_e^i(k) = 1] \leftrightarrow [H^i x_c(k) + K^i u_c(k) \leq W^i]$$

$$x_c \in \mathbb{R}^{n_c}, u_c \in \mathbb{R}^{m_c}, \delta_e \in \{0, 1\}^{n_e}$$

Example: $[\delta=1] \leftrightarrow [x_c(k) \geq 0]$

Computational Hybrid Models

Discrete Hybrid Automaton



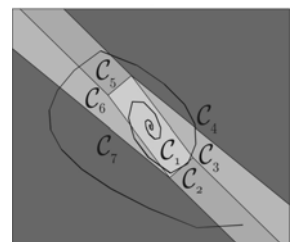
HYSDEL
(Torrise, Bemporad, 2004)

Piecewise Affine (PWA) Systems

$$\begin{aligned} x(k+1) &= A_{i(k)}x(k) + B_{i(k)}u(k) + f_{i(k)} \\ y(k) &= C_{i(k)}x(k) + D_{i(k)}u(k) + g_{i(k)} \\ i(k) &\text{ s.t. } H_{i(k)}x(k) + J_{i(k)}u(k) \leq K_{i(k)} \end{aligned}$$

MLD2PWA
(Bemporad, 2004)

state+input space



(Sontag 1981)

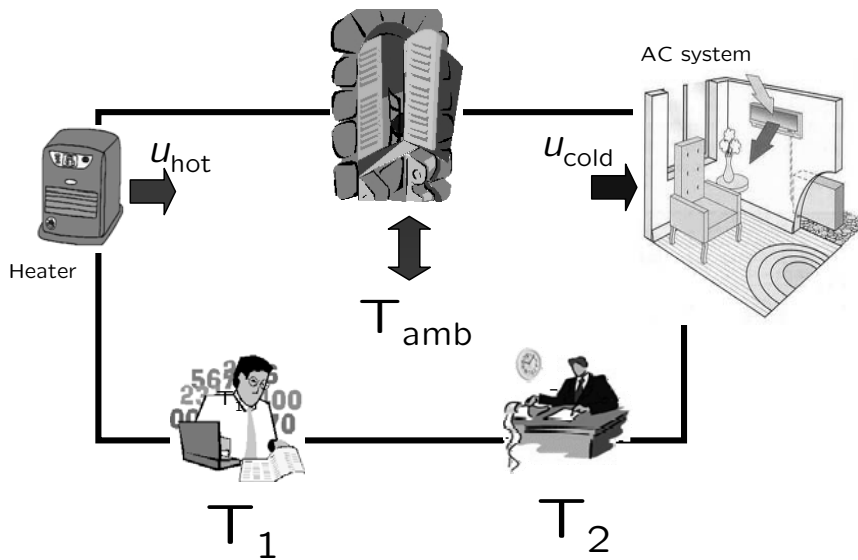
Mixed Logical Dynamical (MLD) Systems

$$\begin{aligned} x(t+1) &= Ax(t) + B_1u(t) + B_2\delta(t) + B_3z(t) + B_5 \\ y(t) &= Cx(t) + D_1u(t) + D_2\delta(t) + D_3z(t) + D_5 \\ E_2\delta(t) + E_3z(t) &\leq E_4x(t) + E_1u(t) + E_5 \end{aligned}$$

(Bemporad, Morari 1999)

The translation from DHA to MLD/PWA is done automatically (using symbolic/mathematical programming tools)

Example: Room Temperature



Hybrid Dynamics

- #1 turns the heater (air conditioning) on whenever he is cold (hot)
- If #2 is cold he turns the heater on, unless #1 is hot
- If #2 is hot he turns the air conditioning on, unless #2 is cold
- Otherwise, heater and air conditioning are off

- $\dot{T}_1 = -\alpha_1(T_1 - T_{amb}) + k_1(u_{hot} - u_{cold})$ (body temperature dynamics of #1)
- $\dot{T}_2 = -\alpha_2(T_2 - T_{amb}) + k_2(u_{hot} - u_{cold})$ (body temperature dynamics of #2)

HYSDEL Model

```

SYSTEM heatcool (
INTERFACE {
STATE { REAL T1 [-10,50];
        REAL T2 [-10,50];
}
INPUT { REAL Tamb [-10,50];
}
PARAMETER {
REAL Ts, alpha1, alpha2, k1, k2;
REAL Thot1, Tcold1, Thot2, Tcold2, Uc, Uh;
}
}
IMPLEMENTATION {
AUX { REAL uhot, ucold;
      BOOL hot1, hot2, cold1, cold2;
}
AD { hot1 = T1>=Thot1;
     hot2 = T2>=Thot2;
     cold1 = T1<=Tcold1;
     cold2 = T2<=Tcold2;
}
DA { uhot = {IF cold1 | (cold2 & ~hot1) THEN Uh ELSE 0};
      ucold = {IF hot1 | (hot2 & ~cold1) THEN Uc ELSE 0};
}
CONTINUOUS { T1 = T1+Ts*(-alpha1*(T1-Tamb)+k1*(uhot-ucold));
              T2 = T2+Ts*(-alpha2*(T2-Tamb)+k2*(uhot-ucold));
}
}
}
    
```



**Hybrid Toolbox
for Matlab**

(Bemporad, 2003-2005)

<http://www.dii.unisi.it/hybrid/toolbox>

```
>>S=mld('heatcoolmodel',Ts)
```

get the MLD model in Matlab

```
>>[XX,TT]=sim(S,x0,U);
```

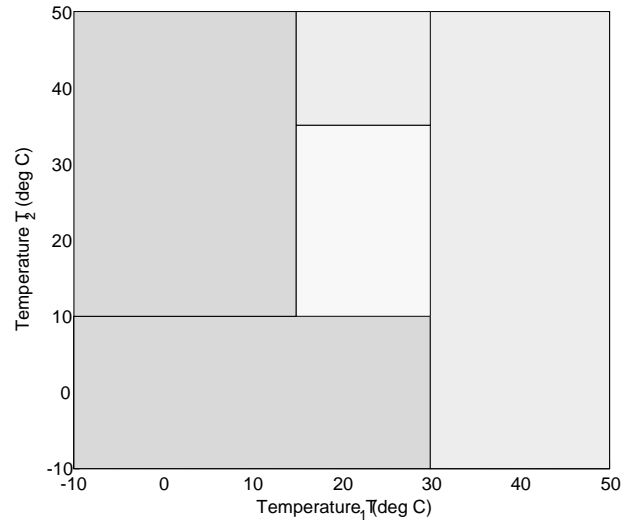
simulate the MLD model

Hybrid PWA Model

- PWA model

$$\begin{aligned}
 x(k+1) &= A_{i(k)}x(k) + B_{i(k)}u(k) + f_{i(k)} \\
 y(k) &= C_{i(k)}x(k) + D_{i(k)}u(k) + g_{i(k)} \\
 i(k) &\text{ s.t. } H_{i(k)}x(k) + J_{i(k)}u(k) \leq K_{i(k)}
 \end{aligned}$$

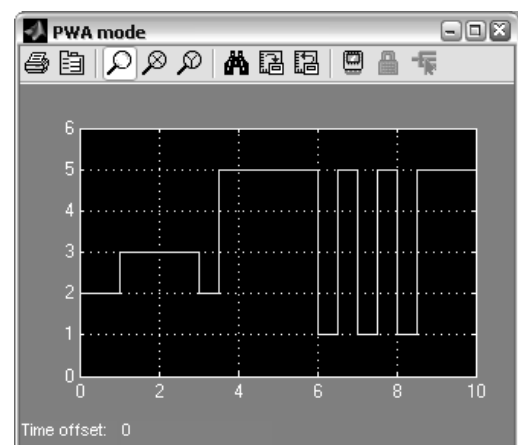
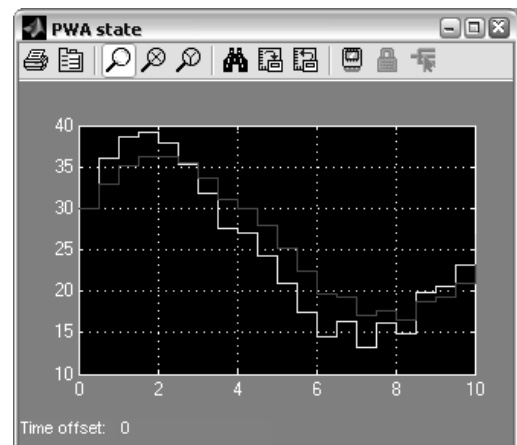
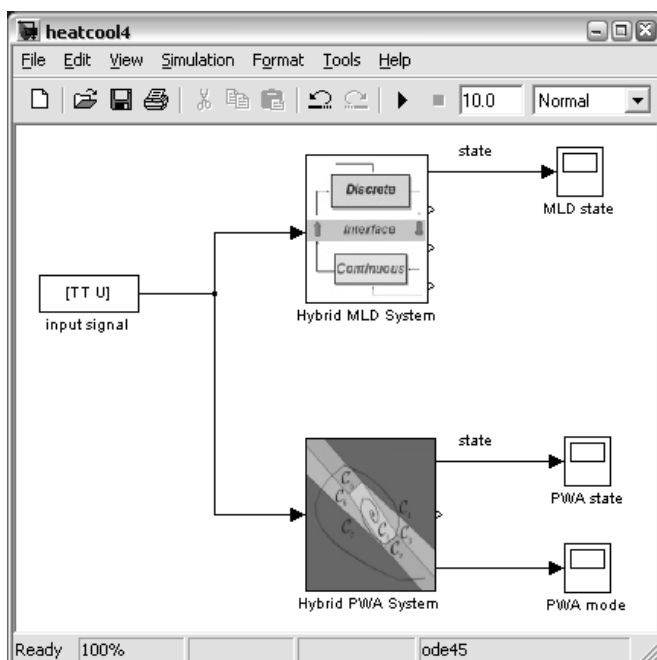
- 2 continuous states:
(temperatures T_1, T_2)
- 1 continuous input:
(room temperature T_{amb})
- 5 polyhedral regions
(partition does not depend on input)



>>P=pwa(S);

$u_{hot} = 0$	$u_{hot} = 0$	$u_{hot} = \bar{U}_H$
$u_{cold} = 0$	$u_{cold} = \bar{U}_C$	$u_{cold} = 0$

Simulation in Simulink



Verification of DHA/MLD/PWA

Verification Algorithm

- **QUERY:** Is the target set X_f reachable after N steps from some initial state $x_0 \in X_0$ for some input profile $u \in U$?
- Computation: Solve the mixed-integer linear program (MILP)

$$\begin{array}{l} \min \quad 0 \\ \text{s.t.} \quad \left\{ \begin{array}{l} x(k+1) = Ax(k) + B_1u(k) + B_2\delta(k) + B_3z(k) \\ E_2\delta(k) + E_3z(k) \leq E_1u(k) + E_4x(k) + E_5 \\ S_uu(k) \leq T_u \quad (u(k) \in U) \\ k = 0, 1, \dots, N-1 \\ \\ S_0x(0) \leq T_0 \quad (x(0) \in X_0) \\ S_fx(N) \leq T_f \quad (x(N) \in X_f) \end{array} \right. \end{array}$$

with respect to $u(0), \delta(0), z(0), \dots, u(N-1), \delta(N-1), z(N-1), x(0)$

- **Alternative solutions:**

- Exploit the special structure of the problem and use polyhedral computation. (Torrise, 2003)
- Use abstractions (LPs) + SAT solvers (Giorgetti, Pappas, 2005)

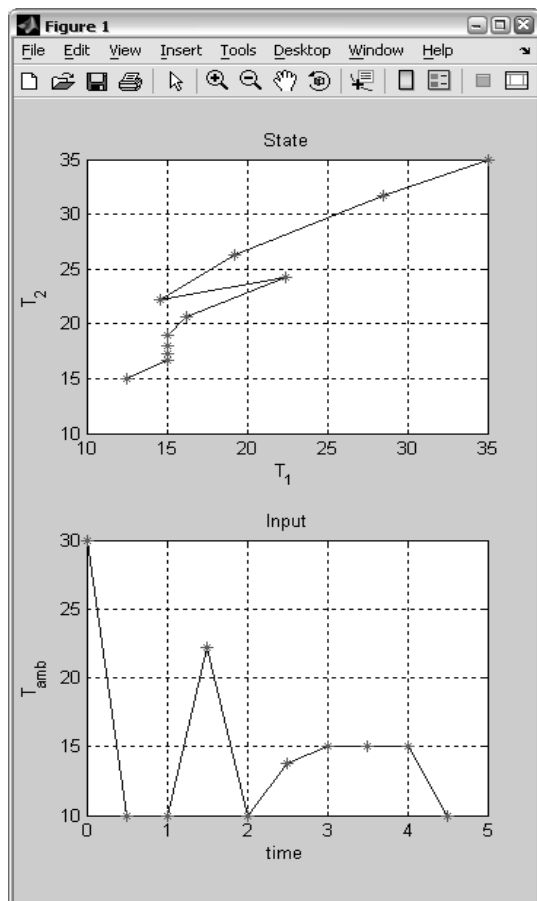
Verification Example

- MLD model: room temperature system
- $X_f = \left\{ \begin{bmatrix} T_1 \\ T_2 \end{bmatrix} : 10 \leq T_1, T_2 \leq 15 \right\}$ (set of unsafe states)
- $X_0 = \left\{ \begin{bmatrix} T_1 \\ T_2 \end{bmatrix} : 35 \leq T_1, T_2 \leq 40 \right\}$ (set of initial states)
- $U = \{T_{\text{amb}} : 10 \leq T_{\text{amb}} \leq 30\}$ (set of possible inputs)
- $N=10$ (time horizon)

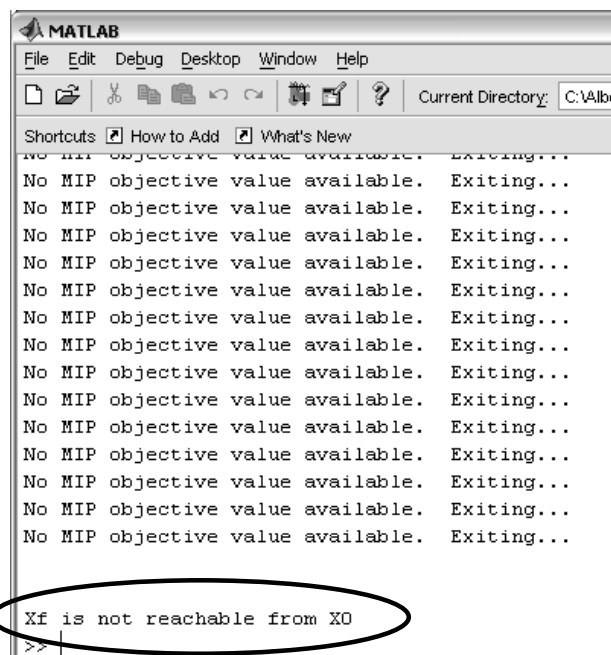


```
>> [flag,x0,U]=reach(S,N,Xf,X0,umin,umax);
```

Verification Example



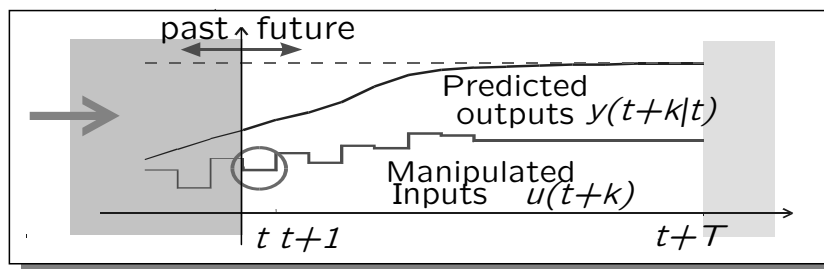
$$U = \{T_{\text{amb}} : 10 \leq T_{\text{amb}} \leq 30\}$$



$$U = \{T_{\text{amb}} : 20 \leq T_{\text{amb}} \leq 30\}$$

Controller Synthesis

Control Strategy: MPC



Model
Predictive (MPC)
Control

- At time t solve with respect to $U \triangleq \{u(t), u(t+1), \dots, u(t+T-1)\}$ the finite-horizon open-loop, optimal control problem:

$$\begin{aligned} & \min_{u(t), \dots, u(t+T-1)} \sum_{k=0}^{T-1} \|R(y(t+k|t) - r(t+k))\|_p + \|Qu(t+k)\|_p \\ & \text{subject to } \begin{cases} \text{MLD or PWA model} \\ x(t|t) = x(t) \end{cases} \end{aligned}$$

$$p = 1, 2, \infty \quad \|v\|_2 = v'v \quad \|v\|_\infty = \max |v_i| \quad \|v\|_1 = \sum v_i$$

- Apply only $u(t) = u^*(t)$ (discard the remaining optimal inputs);
- Repeat the whole optimization at time $t+1$

Hybrid MPC - Example

```
>>refs.x=2;    % just weight state #2
>>Q.x=1;
>>Q.rho=Inf;  % hard constraints
>>Q.norm=2;   % quadratic costs
>>N=2;        % optimization horizon
>>limits.xmin=[25;-Inf];
```

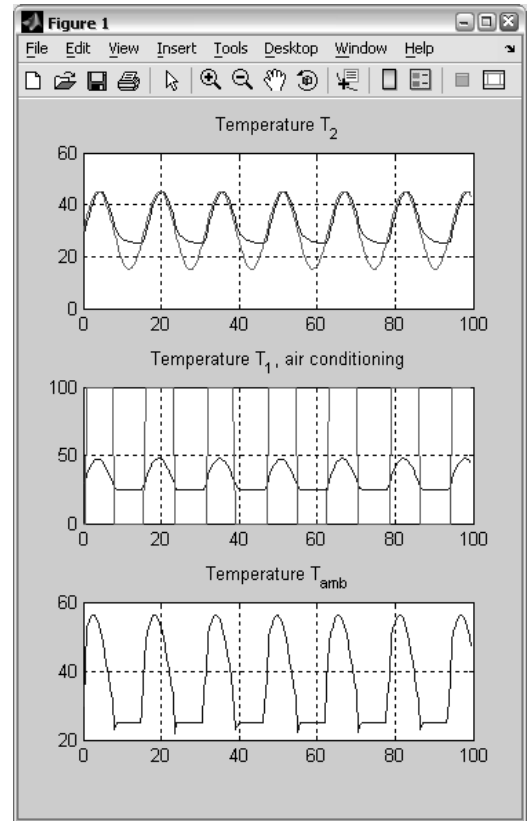
```
>>C=hybcon(S,Q,N,limits,refs);
```

```
>> C
Hybrid controller based on MLD model S <heatcoolmodel.hys>

 2 state measurement(s)
 0 output reference(s)
 0 input reference(s)
 1 state reference(s)
 0 reference(s) on auxiliary continuous z-variables

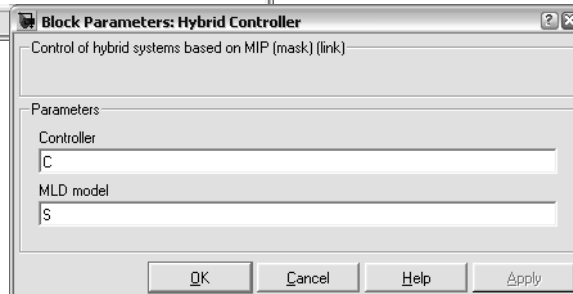
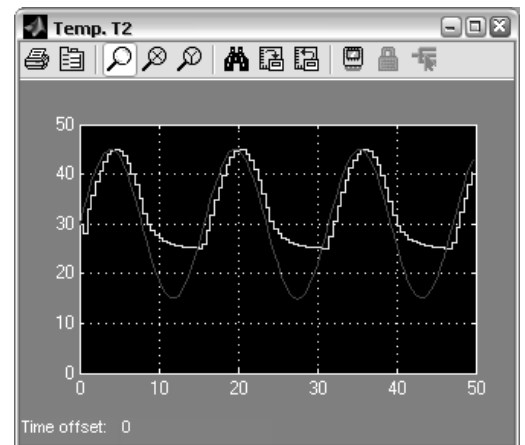
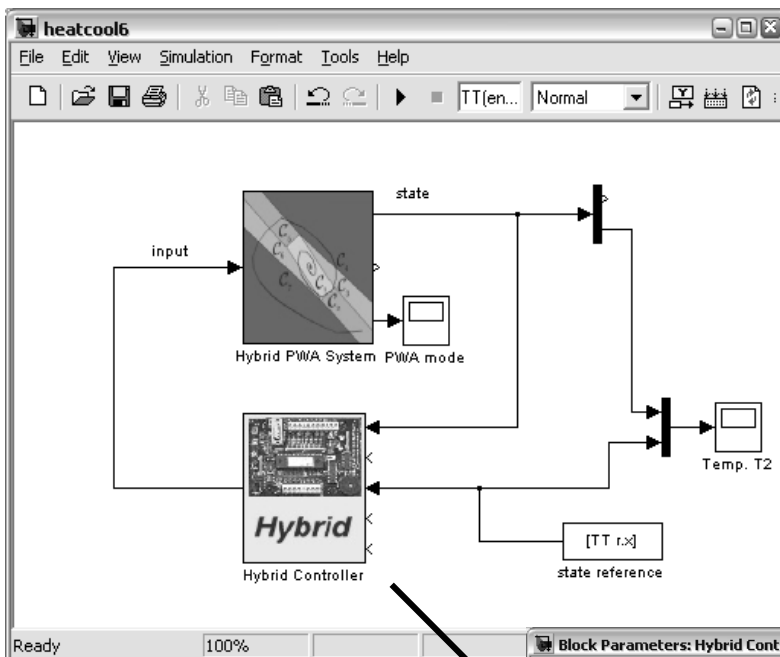
20 optimization variable(s) (8 continuous, 12 binary)
46 mixed-integer linear inequalities
sampling time = 0.5, MILP solver = 'glpk'

Type "struct(C)" for more details.
>>
```



```
>>[XX,UU,DD,ZZ,TT]=sim(C,S,r,x0,Tstop);
```

Hybrid MPC - Example



On-Line vs Off-Line Optimization

$$\min_U J(U, x(t)) = \sum_{k=0}^{T-1} \|Rx(t+k|t)\|_p + \|Qu(t+k)\|_p$$

subject to $\begin{cases} \text{MLD model} \\ x(t|t) = x(t) \end{cases}$

- On-line optimization: given $x(t)$ solve the problem at each time step t .

Mixed-Integer Linear/Quadratic Program (MILP/MIQP)

- Good for large sampling times (e.g., 1 h) / expensive hardware ...
... but not for fast sampling (e.g. 10 ms) / cheap hardware !

- Off-line optimization: solve the MILP/MIQP for all $x(t)$

$$\min_{\zeta} J(\zeta, x(t)) = \begin{cases} f'\zeta & \infty/1\text{-norms} \\ \zeta'H\zeta + f'\zeta & \text{quadratic forms} \end{cases}$$

s.t. $G\zeta \leq W + Fx(t)$

multi-parametric programming

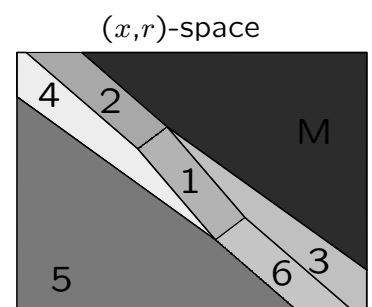
Explicit Hybrid MPC

$$\min_U J(U, x, r) = \sum_{k=0}^{T-1} \|R(y(k) - r)\|_p + \|Qu(k)\|_p$$

subject to $\begin{cases} \text{PWA model} \\ x(0) = x \end{cases}$

- Solution $u(x, r)$ found via a combination of
 - Dynamic programming or enumeration of feasible mode sequences, multiparametric linear or quadratic programming, and polyhedral computation. (Borrelli, Baotic, Bemporad, Morari, 2003) (Mayne, ECC 2001) (Alessio, Bemporad, 2005)
- The MPC controller is piecewise affine in x, r**

$$u(x, r) = \begin{cases} F_1x + E_1r + g_1 & \text{if } H_1 \begin{bmatrix} x \\ r \end{bmatrix} \leq K_1 \\ \vdots & \vdots \\ F_Mx + E_Mr + g_M & \text{if } H_M \begin{bmatrix} x \\ r \end{bmatrix} \leq K_M \end{cases}$$



Note: in the quadratic case the partition may not be fully polyhedral

Explicit Hybrid MPC - Example

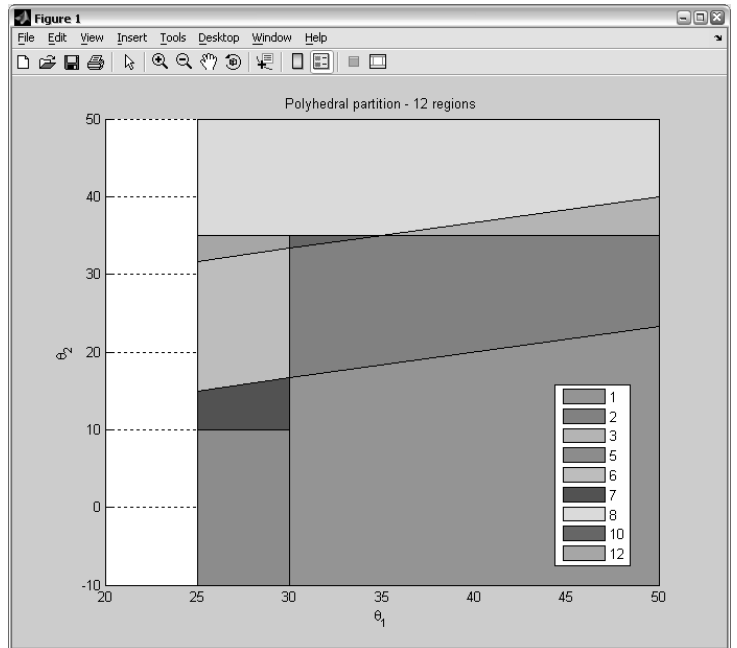
```
>>E=expcon(C,range,options);
```

```
>> E
```

```
Explicit controller (based on hybrid controller C)
 3 parameter(s)
 1 input(s)
 11 partition(s)
sampling time = 0.5
```

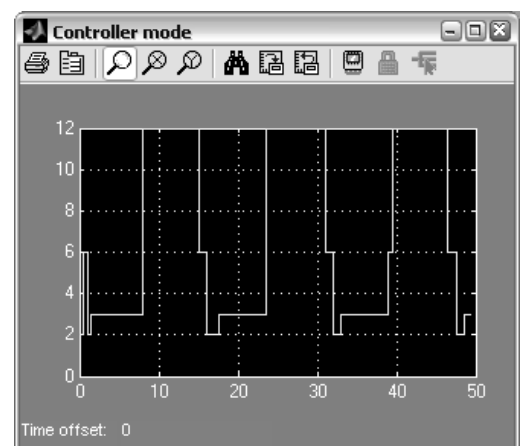
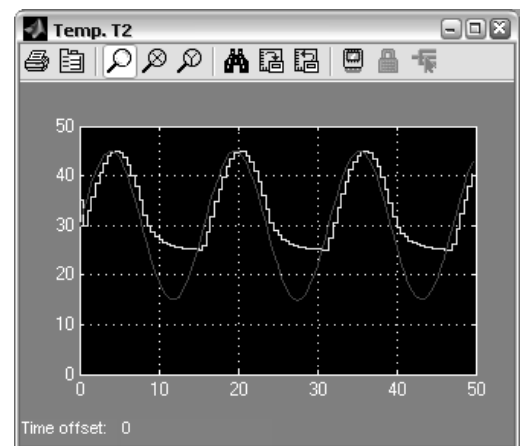
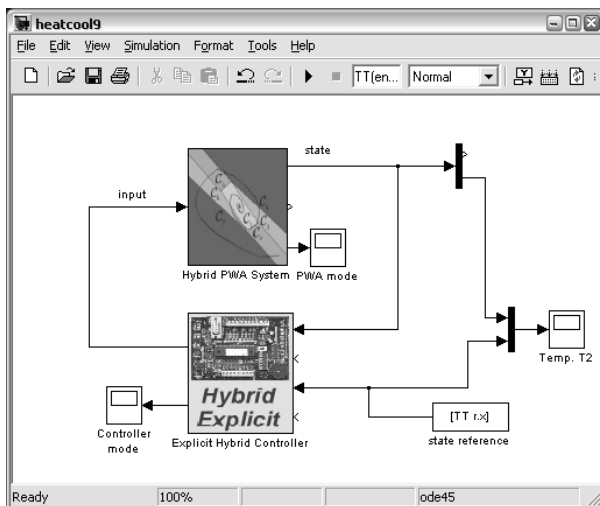
```
The controller is for hybrid systems (tracking)
This is a state-feedback controller.
```

```
Type "struct(E)" for more details.
>>
```



Section in the (T_1, T_2) -space for $T_{ref} = 30$

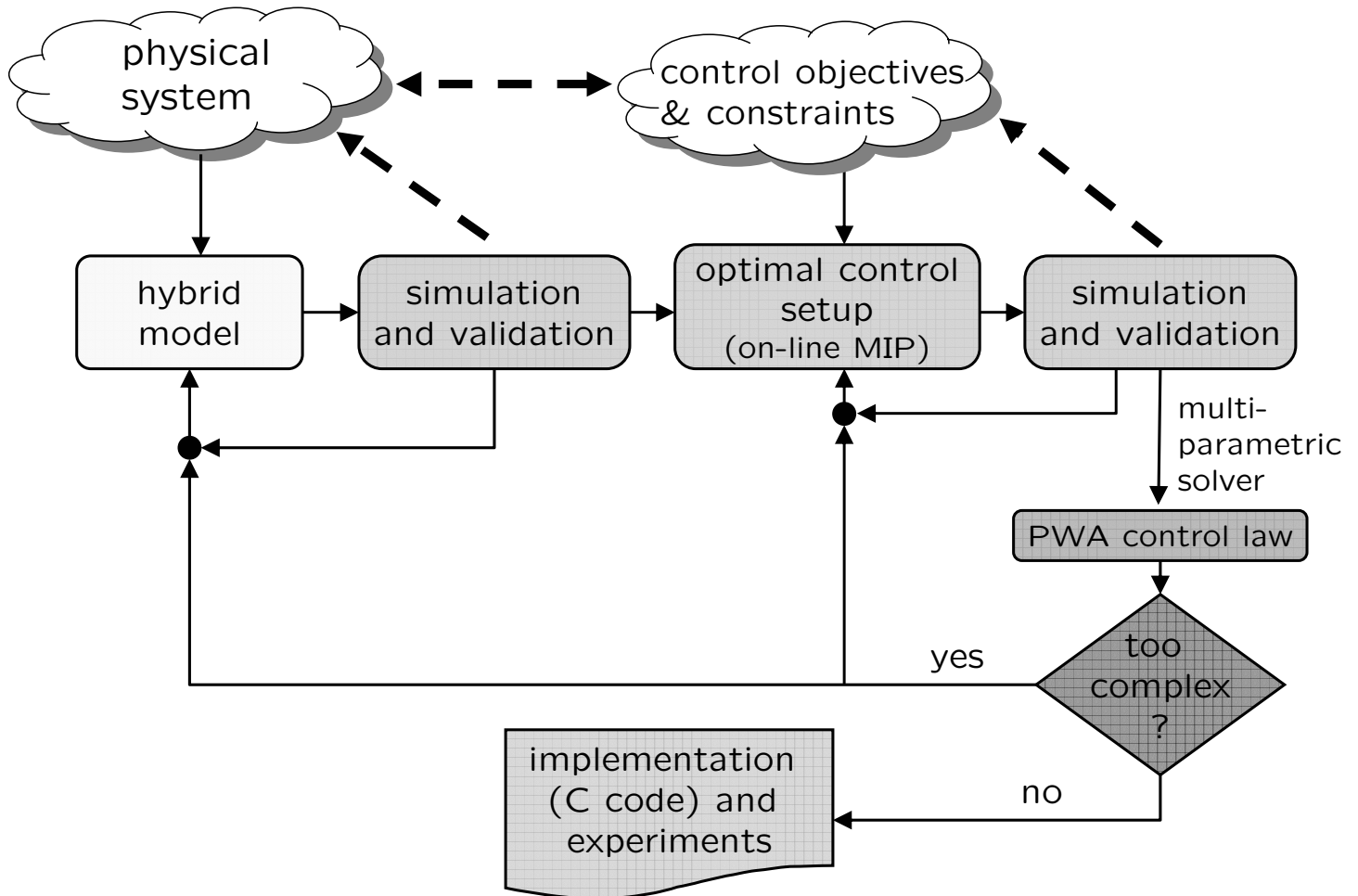
Explicit Hybrid MPC - Example



Generated
C-code

```
#define EXPCON_REG 12
#define EXPCON_NTH 3
#define EXPCON_NYH 2
#define EXPCON_NH 72
#define EXPCON_NF 12
static double EXPCON_F[]={
  -1,0,0,0,-1,0,
  -1,-1,-1,-1,-1,-1,0,-3,-3,
  -3,0,-3,0,0,0,0,0,
  0,0,4,4,4,0,4,0,0,
  0,0,0,0};
static double EXPCON_G[]={
  101.6,1.6,1.6,-1.6,98.4001,0,100,51.6,
  101.6,51.6,48.4,50};
static double EXPCON_H[]={
  0,0,0,-0.00999999,0,-0.0333333,
  0.02,0.00999999,-0.02,0,0,-0.0333333,0.02,0.00999999,
  0,0,-0.02,0.02,0,-1,0.00999999,0,
```

Hybrid Control Design Flow



(Photo: Courtesy Mitsubishi)

Application of Explicit Hybrid MPC to DISC Engine Control

(joint work with N. Giorgetti, I. Kolmanovsky, D. Hrovat)

DISC Engine

States/Controlled outputs:

- Intake manifold pressure (p_m);
- Air-to-fuel ratio (λ);
- Engine brake torque (τ);

Inputs (continuous):

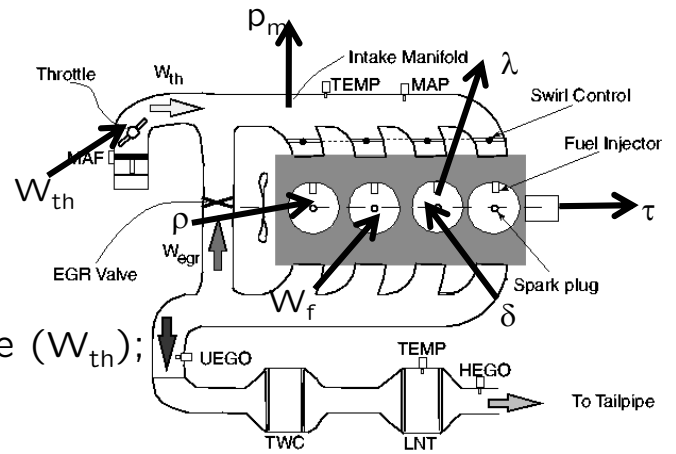
- Air Mass flow rate through throttle (W_{th});
- Mass flow rate of fuel (W_f);
- Spark timing (δ);

Inputs (binary):

- ρ = regime of combustion (homogeneous/stratified);

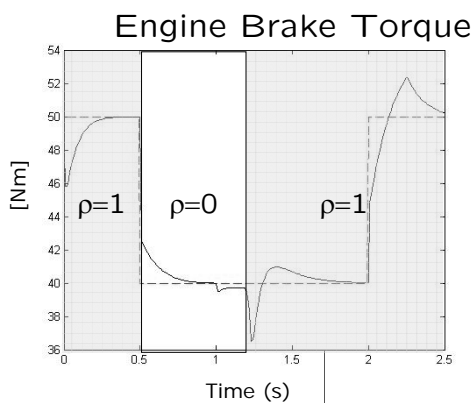
Constraints on:

- Air-to-Fuel ratio (due to engine roughness, misfiring, smoke emiss.)
- Spark timing (to avoid excessive engine roughness)
- Mass flow rate on intake manifold (constraints on throttle)



➔ Dynamic equations are **nonlinear**
Dynamics and constraints **depend on regime ρ** !

Explicit MPC Controller (quadratic costs)



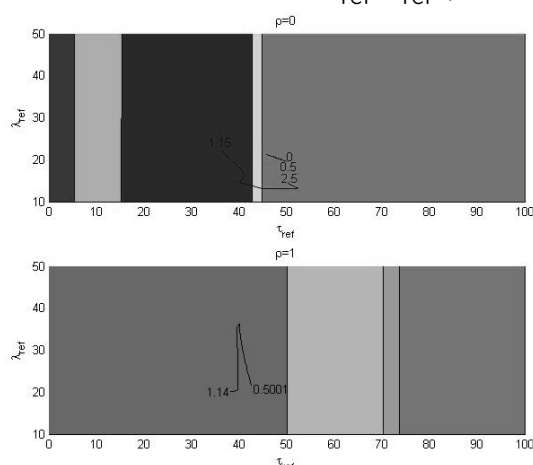
On-line simulations:

- Control horizon $N=1$;
- Simulation time $T=2.5$ s;
- Sampling time $T_s=10$ ms;
- CPU time ≈ 8 s;
(on an Intel Centrino 1.2 GHz, 640 Mb RAM with Cplex 9.01)

➔ ≈ 32 ms per time step

Not directly implementable !

Cross-section in the $\tau_{ref}-\lambda_{ref}$ plane



Explicit simulations:

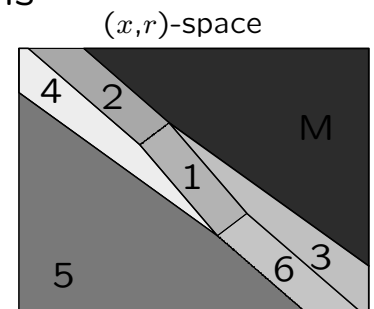
- Control horizon $N=1$;
 - 9 Parameters;
 - CPU time ≈ 0.52 s
- ➔ **75 Partitions**
 ≈ 2 ms per time step

Implementable !

Conclusions

- **Discrete hybrid automata** are simple yet versatile models of hybrid systems, and lead immediately computationally-useful models
- **Optimization-based control** handles performance specs and constraints in a natural and direct way. Quite complex hybrid systems can be controlled using on-line mixed-integer programming
- **Piecewise affine MPC controllers** can be synthesized, off-line, and implemented as look-up tables of linear gains

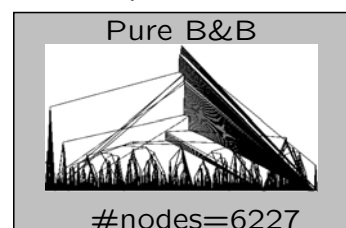
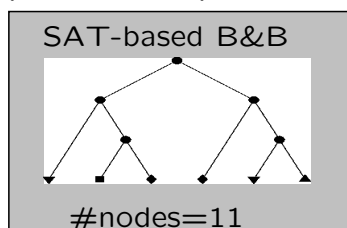
$$u(x, r) = \begin{cases} F_1x + E_1r + g_1 & \text{if } H_1 \begin{bmatrix} x \\ r \end{bmatrix} \leq K_1 \\ \vdots & \vdots \\ F_Mx + E_Mr + g_M & \text{if } H_M \begin{bmatrix} x \\ r \end{bmatrix} \leq K_M \end{cases}$$



- **Hybrid Toolbox for Matlab** available to assist controller design: modeling, simulation, verification, MPC, code generation

Ongoing Research

- **Logic-based methods:** use combined SAT+LP to largely improve computation performance of optimal control/verification



(N. Giorgetti)

- **Stochastic hybrid models:** (robust) optimal control can be solved using mixed-integer programming

(Di Cairano, HSCC05)

- **Event-based optimal control of hybrid systems:** index k denotes events occurring in piecewise-affine continuous-time systems, rather than discrete time

(Di Cairano, Julvez)

	N	t_s	t_{cpu} (sec.)	t_{viol} (time units)	$t_{viol}^{(sup)}$ (time units)
optimal control train-gate system	5	20.00	0.45	3.82	40.00
	6	16.66	1.46	21.83	33.32
	10	10.00	8.58	9.82	20.00
	15	6.66	66.77	6.55	13.32
	20	5.00	747.14	4.82	10.00
	cont.time		1.09	—	—

The End

MPC controller - SIMO
DC-Servomotor
Hybrid Toolbox